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60 Years

Atoms for Peace and Development

Fission applications: reactor physics

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Nuclear Data Section



- Introduction
- Fission processes
 - Spontaneous, particle induced
 - Cross sections
 - Total and partials
 - Emitted particle yields and spectra
 - Prompt, delayed; independent and cumulative
 - Nu, nubar, prompt fission neutron spectra
 - Fast and thermal
- Nuclear data libraries and processing issues
- Reactor parameters and associated uncertainty
- Fissions processes modelling in reactor physics:
 - Neutronics; reactor engineering
 - Terminologies: pcm, mill-k, millinile, millirho
- Reactor types, piles, criticality issues
 - Deterministic
 - Monte Carlo
- Neutron balance and neutron maps
 - Pin power, Power maps
 - Production, absorption and leakage
- Reactor anti-neutrino anomaly



Nuclear landscape: elemental periodic table

Periodic Table of the Elements

1 H Hydrogen 1.008																	2 He Helium 4.003
3 Li Lithium 6.941	4 Be Beryllium 9.012											5 B Boron 10.811	6 C Carbon 12.011	7 N Nitrogen 14.007	8 O Oxygen 15.999	9 F Fluorine 18.998	10 Ne Neon 20.180
11 Na Sodium 22.990	12 Mg Magnesium 24.305											13 Al Aluminum 26.982	14 Si Silicon 28.086	15 P Phosphorus 30.974	16 S Sulfur 32.066	17 Cl Chlorine 35.453	18 Ar Argon 39.948
19 K Potassium 39.098	20 Ca Calcium 40.078	21 Sc Scandium 44.956	22 Ti Titanium 47.867	23 V Vanadium 50.942	24 Cr Chromium 51.996	25 Mn Manganese 54.938	26 Fe Iron 55.845	27 Co Cobalt 58.933	28 Ni Nickel 58.693	29 Cu Copper 63.546	30 Zn Zinc 65.38	31 Ga Gallium 69.723	32 Ge Germanium 72.631	33 As Arsenic 74.922	34 Se Selenium 78.971	35 Br Bromine 79.904	36 Kr Krypton 84.798
37 Rb Rubidium 84.468	38 Sr Strontium 87.62	39 Y Yttrium 88.906	40 Zr Zirconium 91.224	41 Nb Niobium 92.906	42 Mo Molybdenum 95.95	43 Tc Technetium 98.907	44 Ru Ruthenium 101.07	45 Rh Rhodium 102.906	46 Pd Palladium 106.42	47 Ag Silver 107.868	48 Cd Cadmium 112.414	49 In Indium 114.818	50 Sn Tin 118.711	51 Sb Antimony 121.760	52 Te Tellurium 127.6	53 I Iodine 126.904	54 Xe Xenon 131.294
55 Cs Cesium 132.905	56 Ba Barium 137.328	57-71 Lanthanides	72 Hf Hafnium 178.49	73 Ta Tantalum 180.948	74 W Tungsten 183.84	75 Re Rhenium 186.207	76 Os Osmium 190.23	77 Ir Iridium 192.217	78 Pt Platinum 195.085	79 Au Gold 196.967	80 Hg Mercury 200.592	81 Tl Thallium 204.383	82 Pb Lead 207.2	83 Bi Bismuth 208.980	84 Po Polonium [209]	85 At Astatine [210]	86 Rn Radon 222.018
87 Fr Francium 223.020	88 Ra Radium 226.025	89-103 Actinides	104 Rf Rutherfordium [261]	105 Db Dubnium [262]	106 Sg Seaborgium [266]	107 Bh Bohrium [264]	108 Hs Hassium [277]	109 Mt Meitnerium [278]	110 Ds Darmstadtium [281]	111 Rg Roentgenium [280]	112 Cn Copernicium [285]	113 Nh Nihonium [286]	114 Fl Flerovium [289]	115 Mc Moscovium [289]	116 Lv Livermorium [293]	117 Ts Tennessine [294]	118 Og Oganesson [294]

57 La Lanthanum 138.905	58 Ce Cerium 140.116	59 Pr Praseodymium 140.908	60 Nd Neodymium 144.243	61 Pm Promethium 144.913	62 Sm Samarium 150.36	63 Eu Europium 151.964	64 Gd Gadolinium 157.25	65 Tb Terbium 158.925	66 Dy Dysprosium 162.500	67 Ho Holmium 164.930	68 Er Erbium 167.259	69 Tm Thulium 168.934	70 Yb Ytterbium 173.055	71 Lu Lutetium 174.967
89 Ac Actinium 227.028	90 Th Thorium 232.038	91 Pa Protactinium 231.036	92 U Uranium 238.029	93 Np Neptunium 237.048	94 Pu Plutonium 244.064	95 Am Americium 243.061	96 Cm Curium 247.070	97 Bk Berkelium 247.070	98 Cf Californium 251.080	99 Es Einsteinium [254]	100 Fm Fermium 257.095	101 Md Mendelevium 258.1	102 No Nobelium 259.101	103 Lr Lawrencium [262]

Alkali Metal	Alkaline Earth	Transition Metal	Basic Metal	Semimetal	Nonmetal	Halogen	Noble Gas	Lanthanide	Actinide
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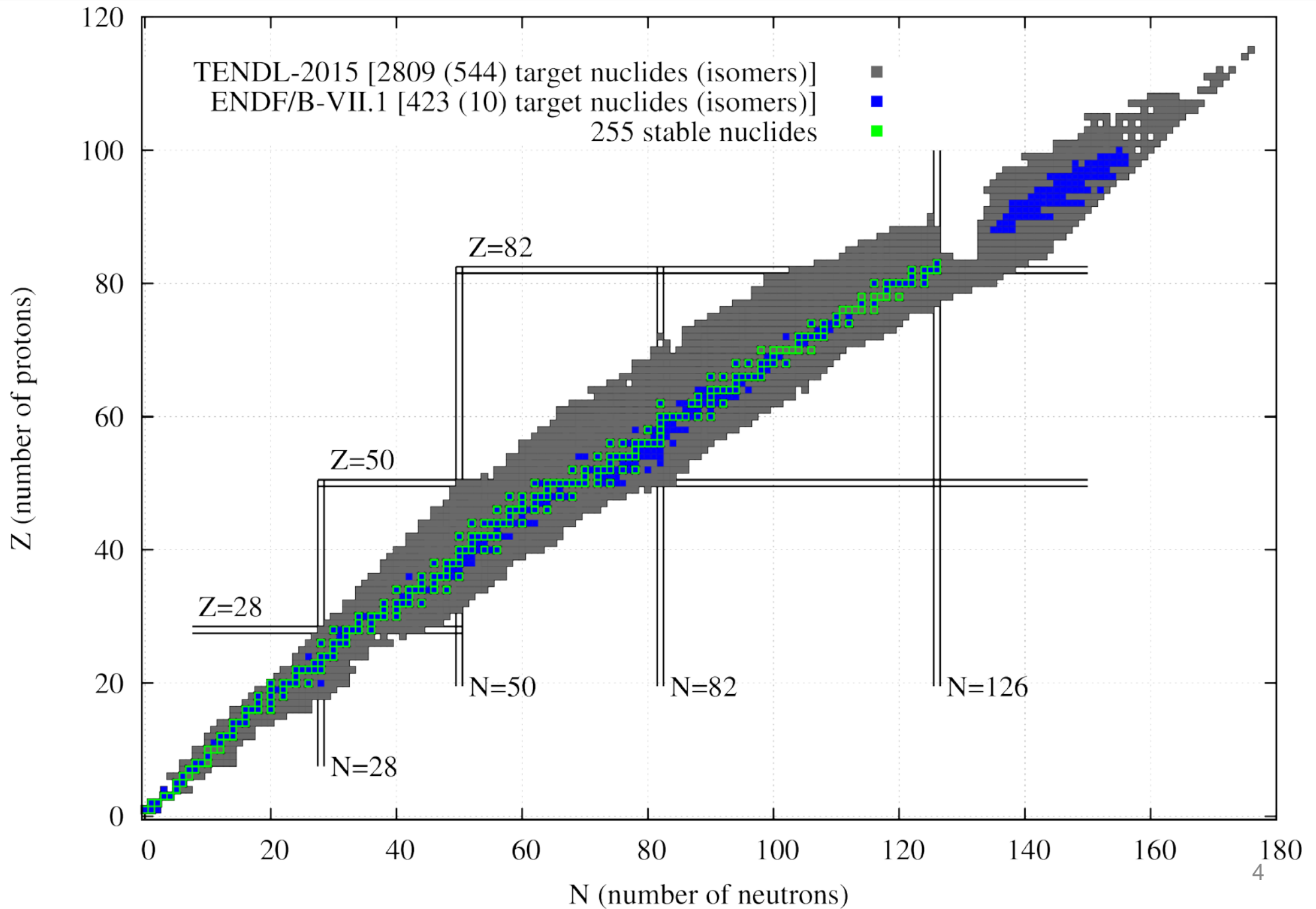


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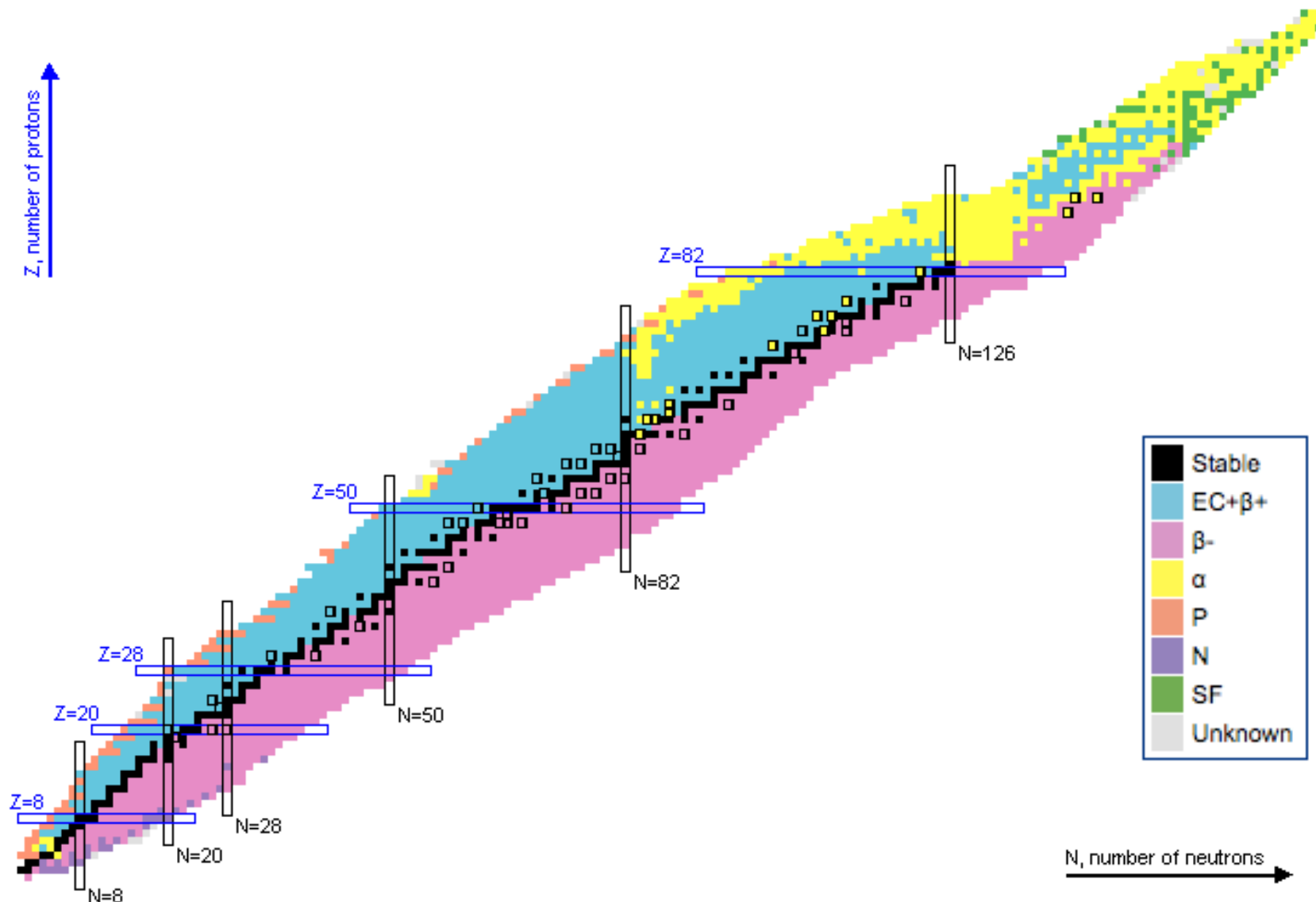
Nuclear landscape: Isotopic targets





Nuclear landscape: decay data

3873 isotopes (23 decay modes; 7 single and 16 multi-particle ones)





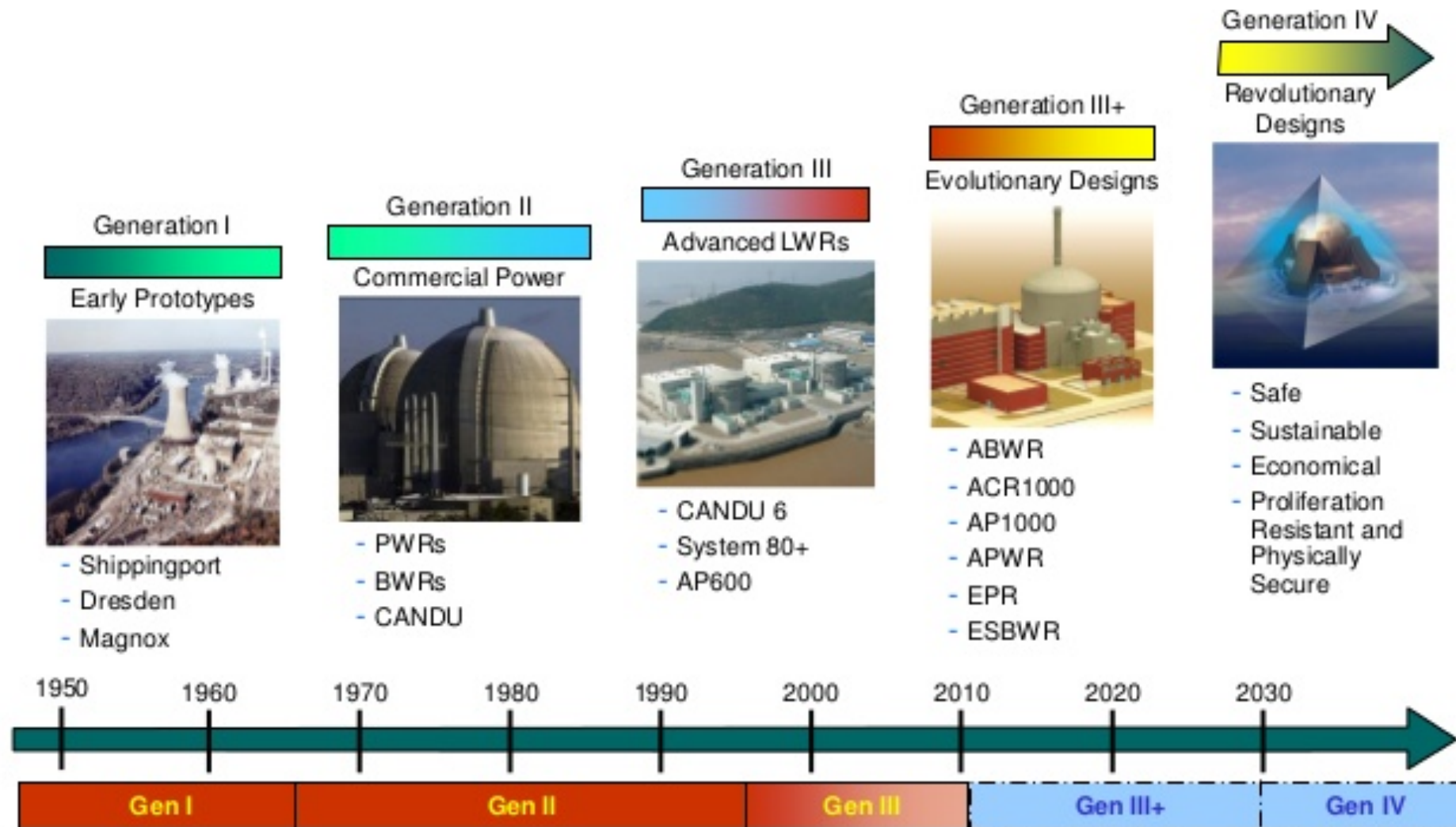
- 1000 MWe, 2900 MWth Typical, 3-4 M€
- Fuel enrichment: 1.8 – 2.4 – 3.1 % mass, 82 ton of UO_2
- $3.1 \cdot 10^{10}$ fission/s = $624 \cdot 10^{10}$ MeV/s ~ 1 Watt
- Heavy isotope production: in order Pu239, U236, Pu240, Pu241, Np-237, Pu242,...
- Pressure 155 bar, T_{in} 292 C, T_{out} +53 C
- Combustion: 33 – 45.000 Mwd/Te
- Mean power
 - assembly 17.7 MW
 - pin 67,2 kW
 - Linear 180 W/cm
 - Surface 60 W/cm²
 - Volume 338.6 W/cm³

444 (96) power
reactors in the
World (March 2017)



• Types:	Operating	Planned
– LWR's:		
• PWR	287	77
• BWR	78	6
– Gas cooled, GCR's:	14	1
– Heavy water, PHWR's:	48	9
– Graphite moderated, LGR's	15	0
– Liquid metal cooled, LMFR, LMR	2	3
– Total	444	96
– No longer in service	156	
– Research reactors, piles 768 (-360)	216	11

- GEN IV = Sodium Fast R's, Very High Temperature R (triso), Small Modular R's, Molten Salt R's

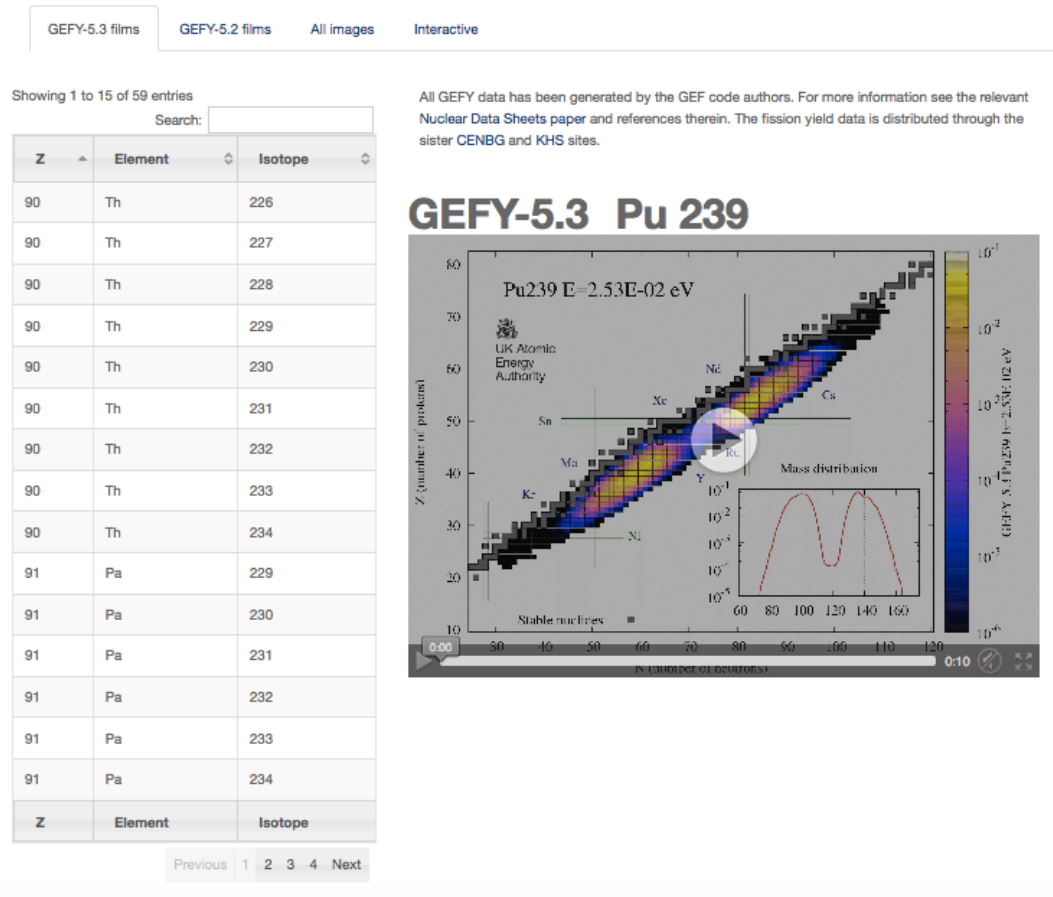


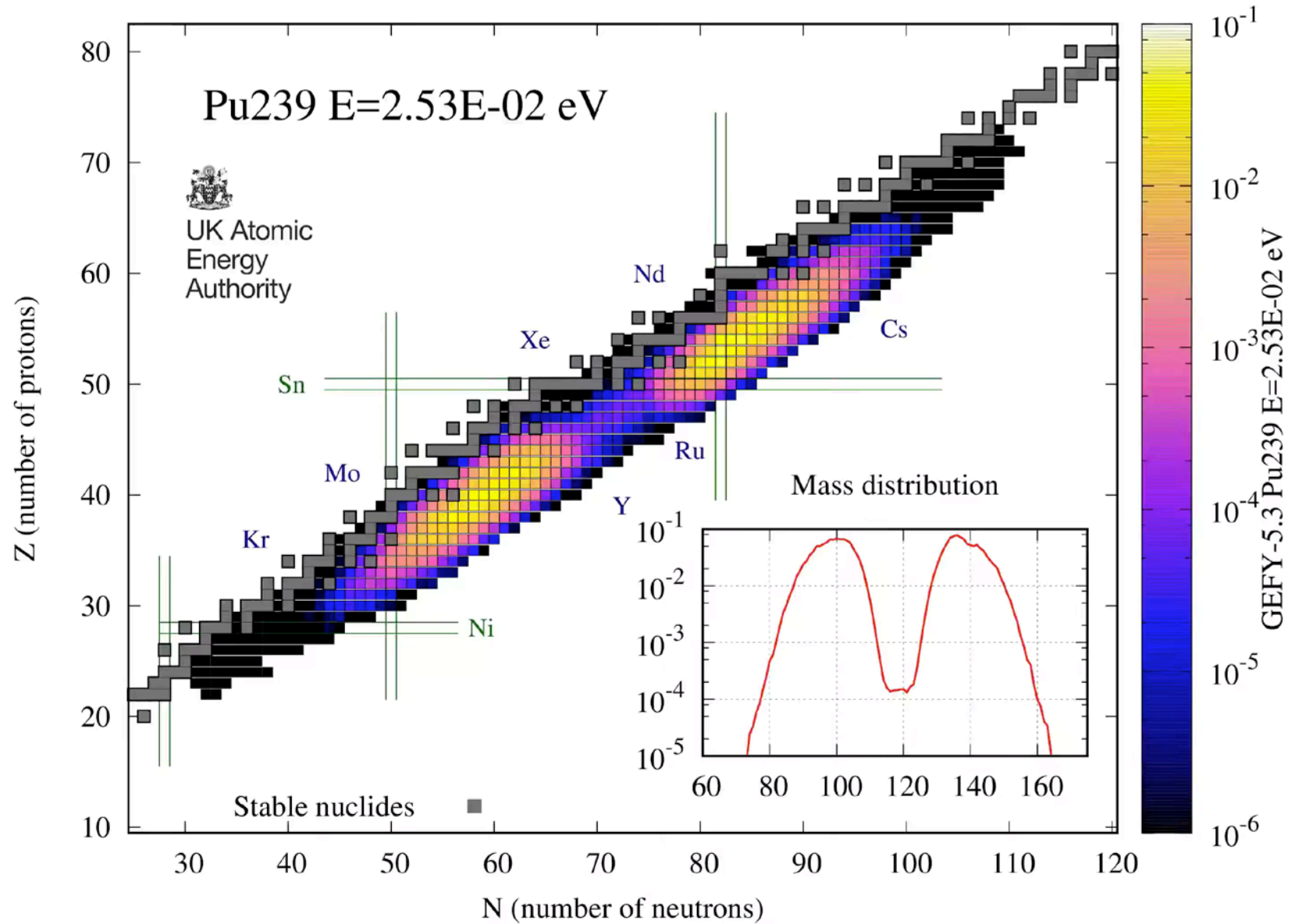


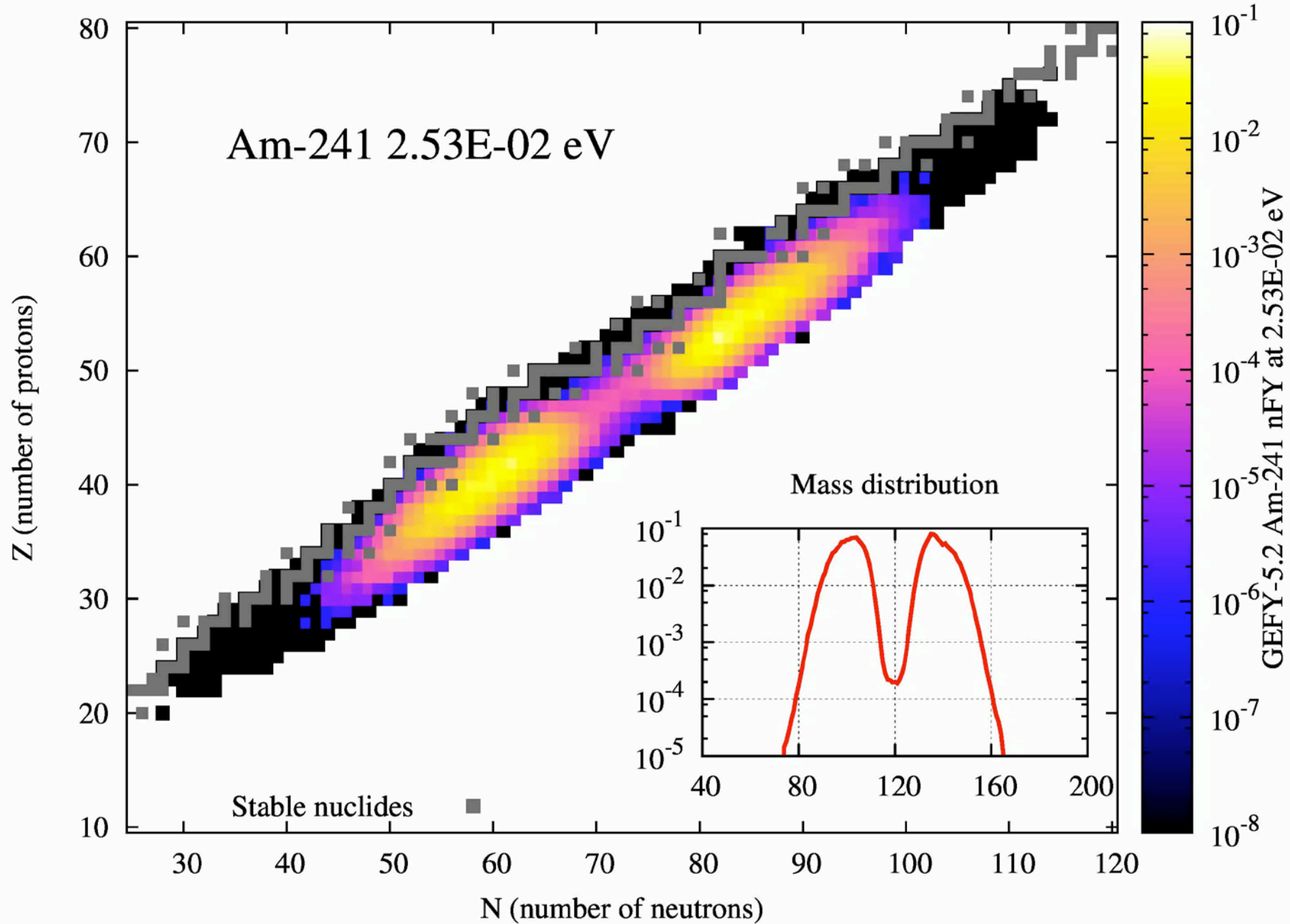
- The importance, treatment of the fission processes differs depending on the applications, but the physic principles underlying them do not
 - fission cross-sections
 - energy dependence, fission chances
 - prompt, delayed neutron multiplicities
 - prompt, delayed emitted neutron spectra
 - fission products yields for typical reactor applications @ thermal
 - prompt, delayed gamma radiations
- For reactor physics fission is a must (to bank 200 MeV per event) but it faces stiff competition (fortunately) from another usually open channel in the same energy range: radiative capture
- In the fuel UO_2 , fission is on U^{235} , while capture is on U^{238}

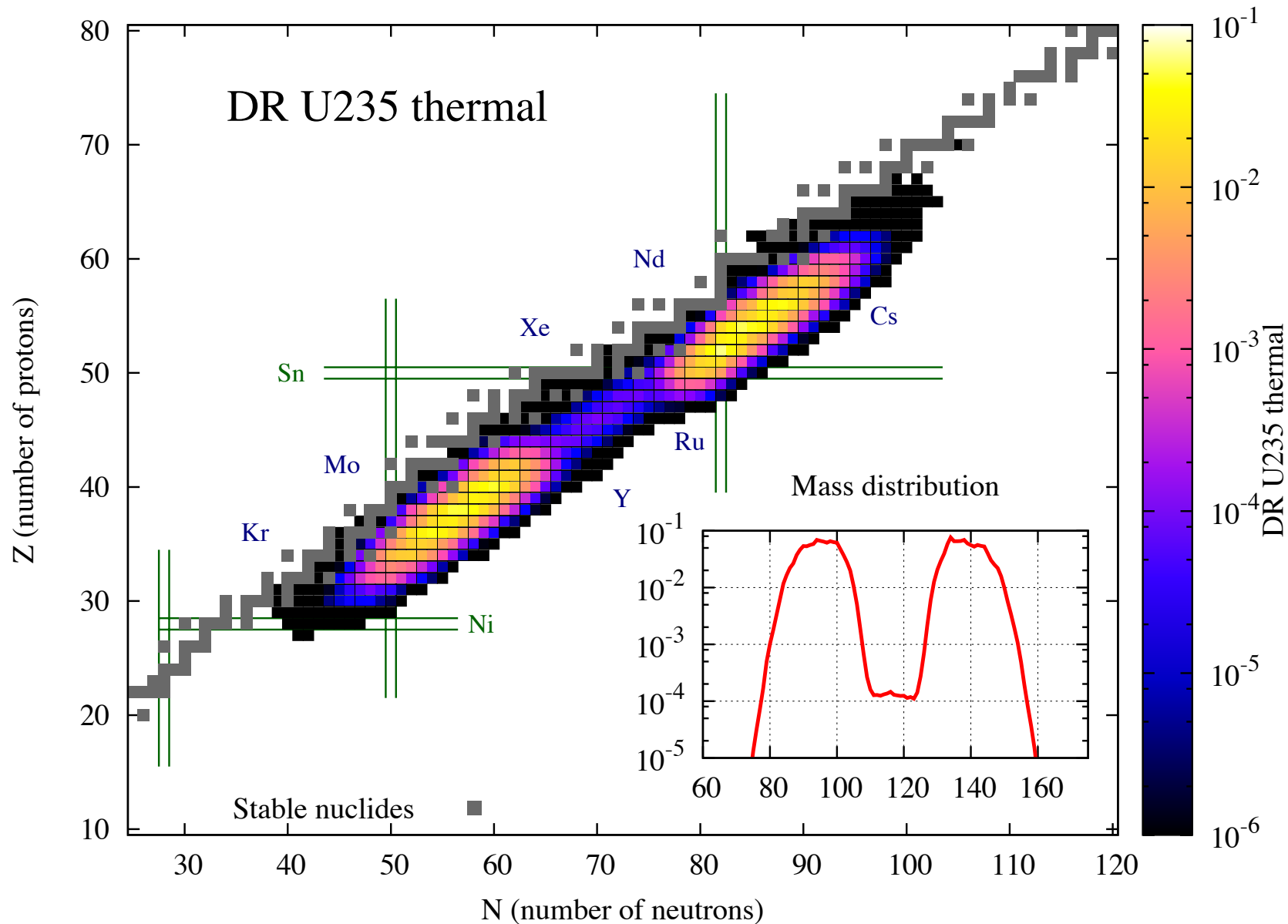
- The importance, treatment of the fission processes differs depending on the applications, what is missing:
 - isotropic, really all events !!
 - fission fragments angular/energy distributions
 - time dependent energy release rates
 - multi-chance fission $(n,n'f)$, $(n,2n'f)$,
 - fission on non-actinides, the lesser fissile
- For reactor physics fission, all the above are of little interest, what is in fact important are
 - the energy release(s) and fission neutron maps during operation and shortly thereafter (accidental scenarios also)
 - the fuel burnup rate, the poisonous fission fragments that capture the neutron that should induce another fission

- Searchable database of fission yield data with visualizations
- Plotly based interactive data interrogation in development
- There are some benefits in scrutinizing the data



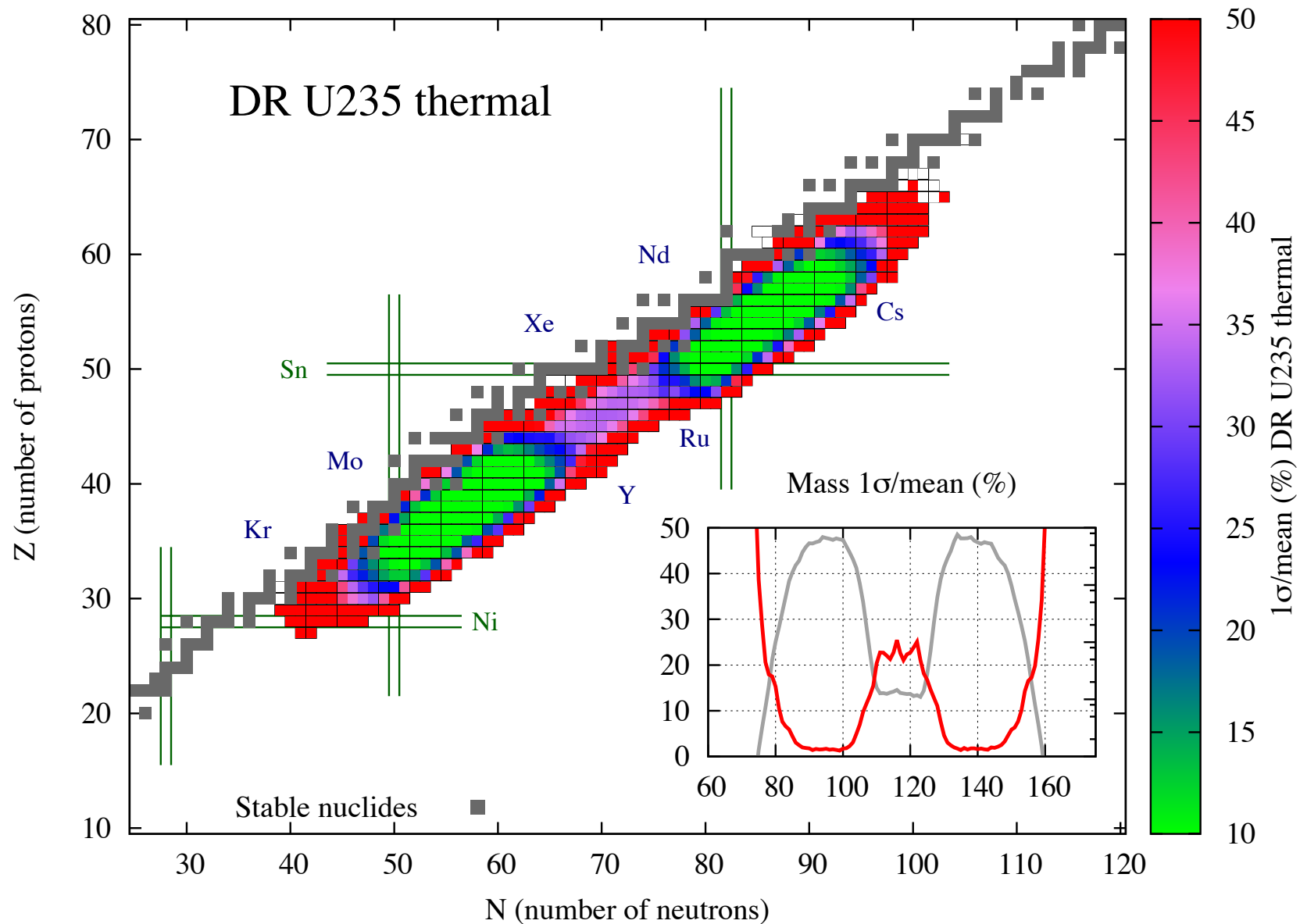






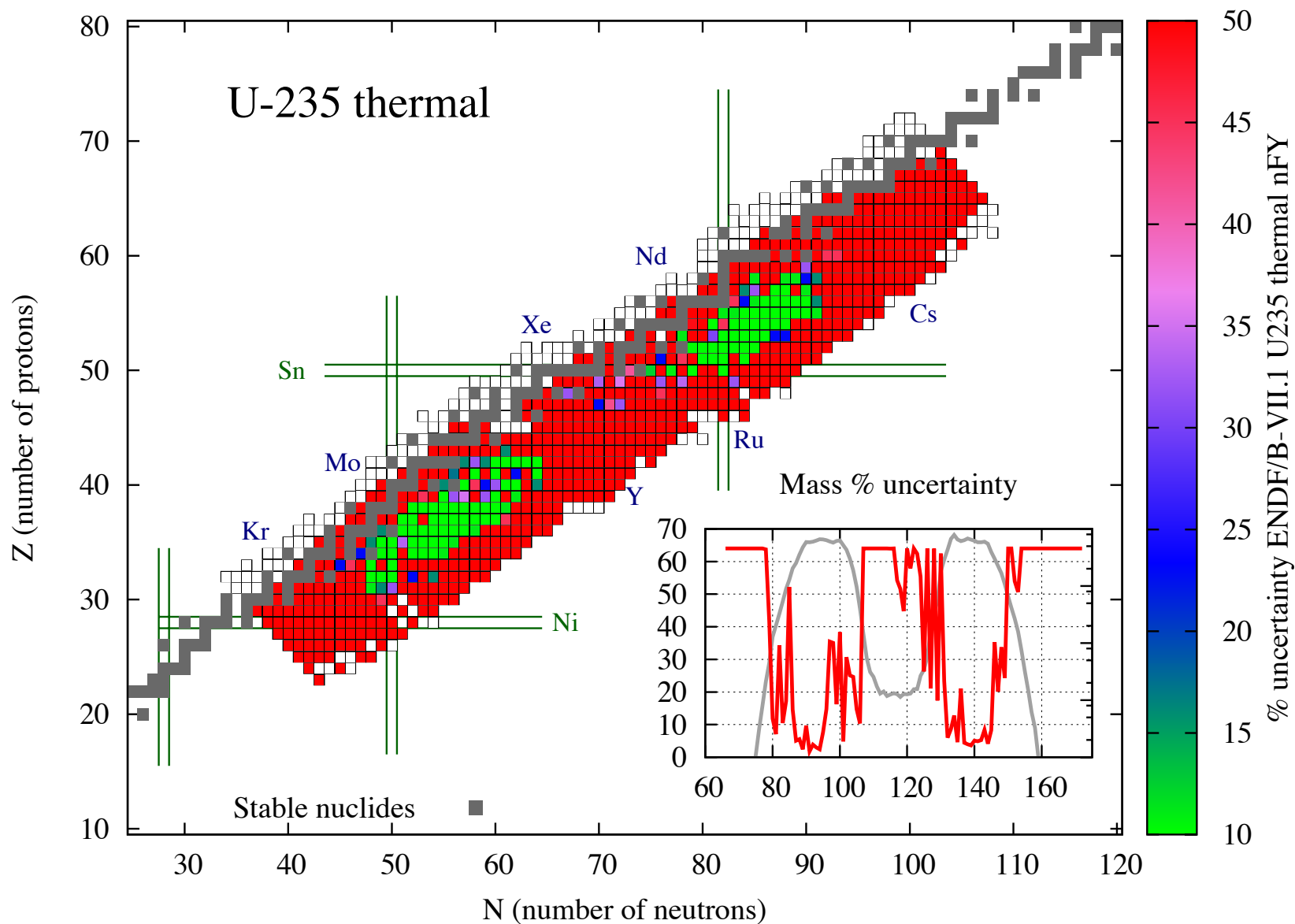


U235 FY's uncertainty @ 0.0253 eV



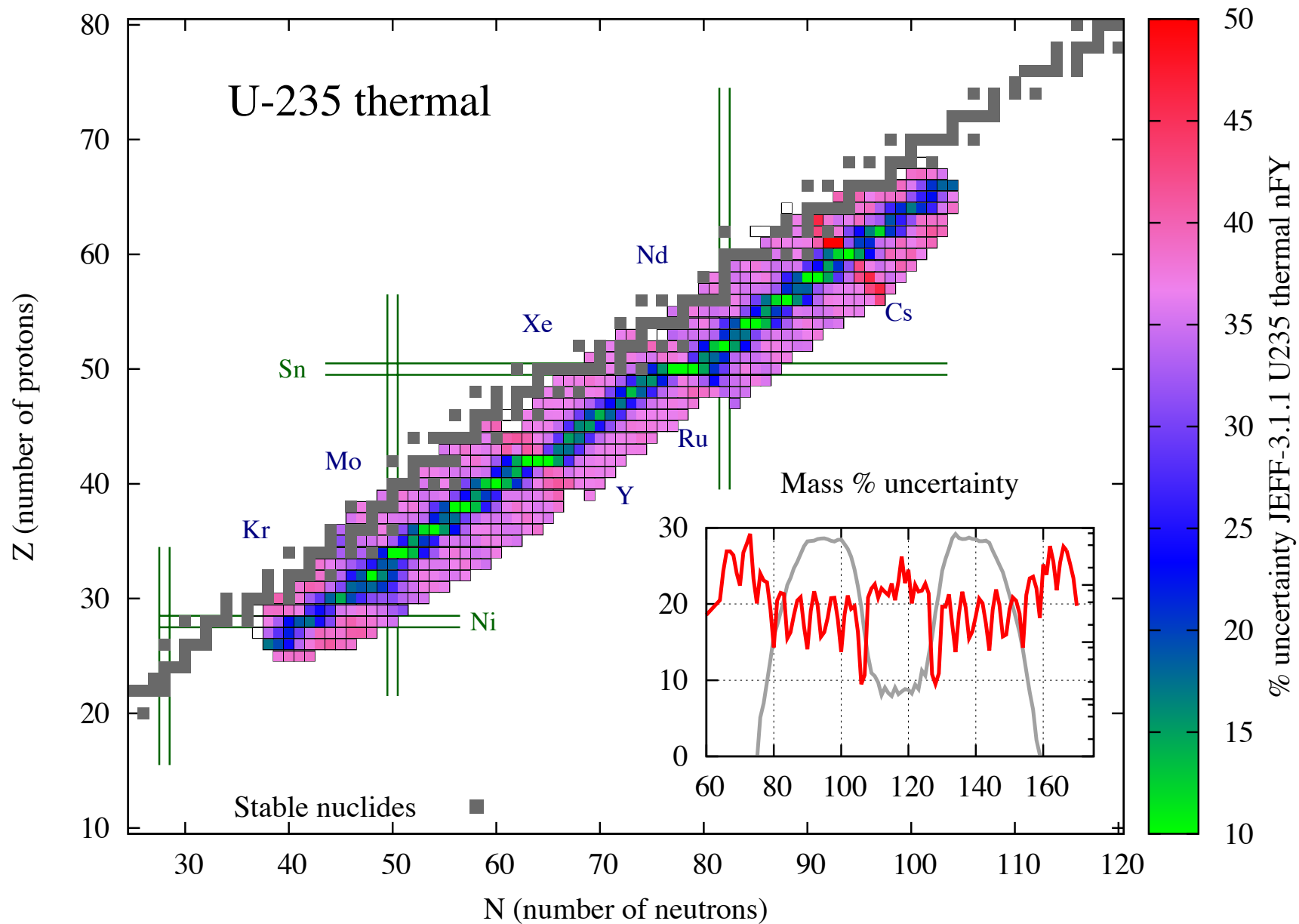


U235 FY's uncertainty @ 0.0253 eV





U235 FY's uncertainty @ 0.0253 eV



Pu²³⁹ fission pulse

Time: 0.000 seconds
Total Decay Heat (kW/kg): 7.653E-04





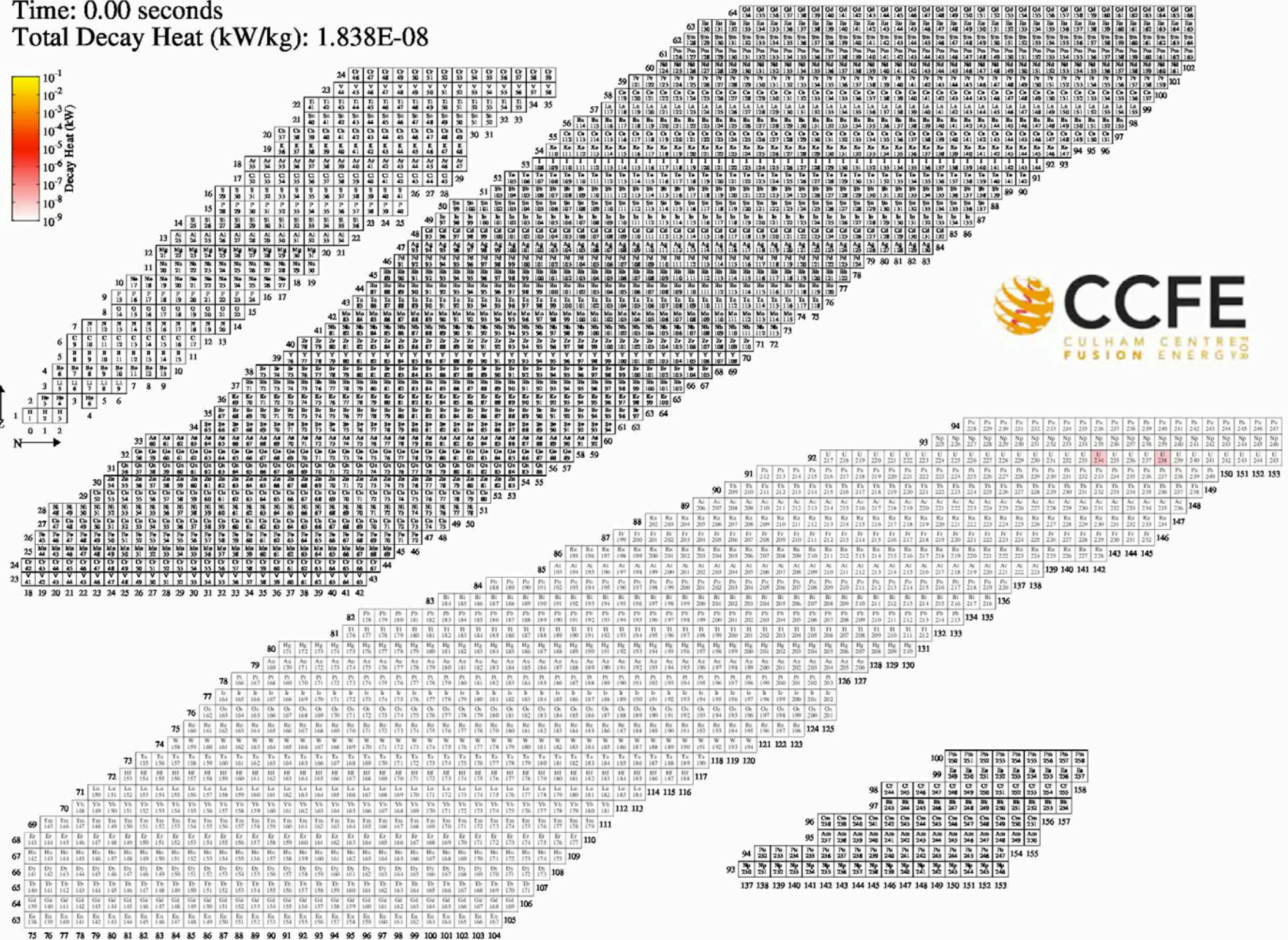
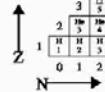
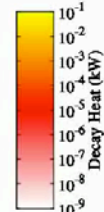
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U235 Fission, 1 year

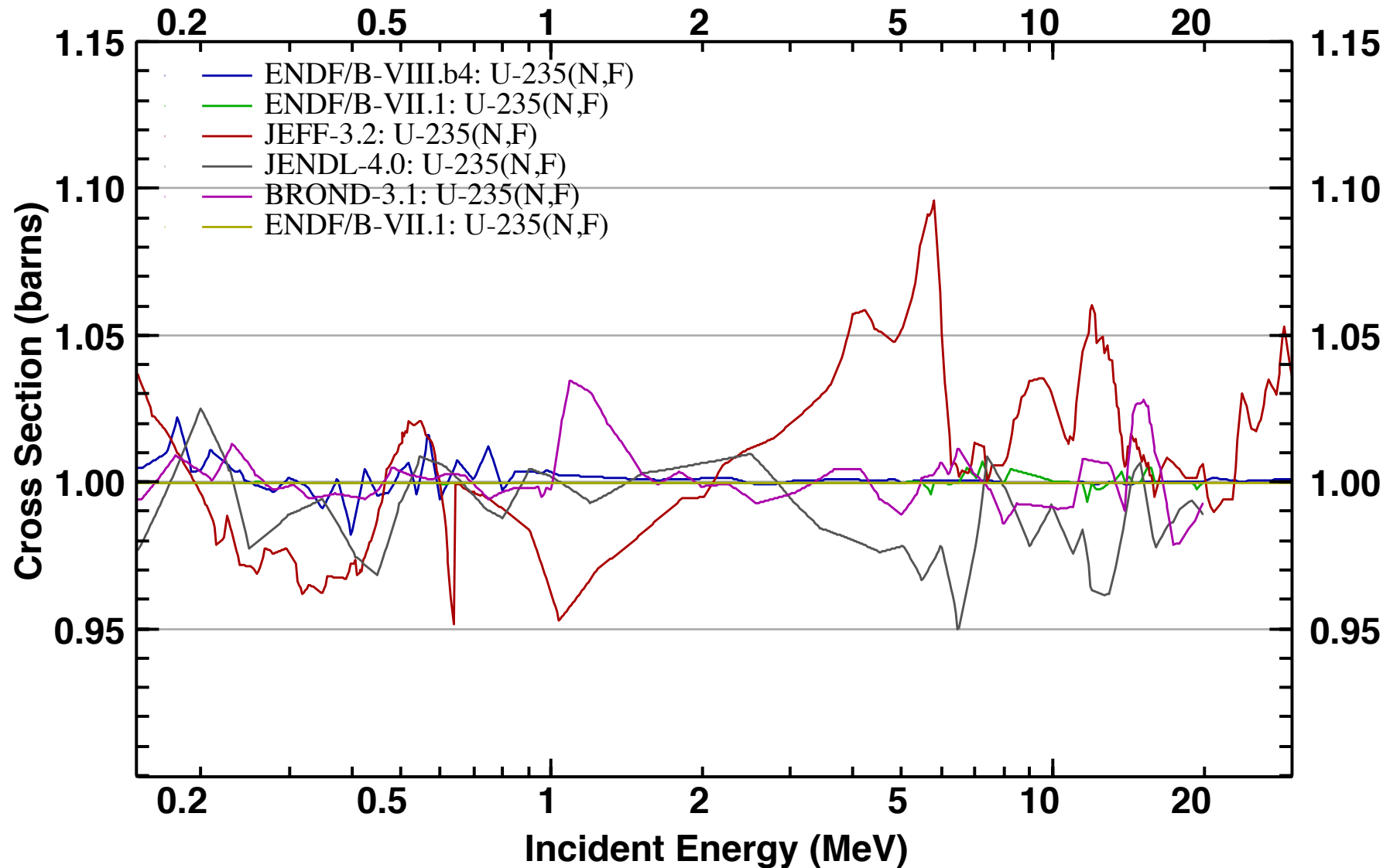
Time: 0.00 seconds

Total Decay Heat (kW/kg): 1.838E-08





Fission cross section(s) in files



- ENDF/B-VII.1, JENDL-4.0, JEFF-3.2, TENDL-2015, GEFY...
 - fission cross sections mf-3 mt-18,19-21,38
 - multiplicities mf-1 mt-452, 455 delayed,456 prompt
 - energy releases for fission mf-1 mt-458
 - neutrons spectra mf-5 or mf-6

- nFYs and sFYs mf-8 mt-454,459
 - independant and cumulative fission yields
 - Incident-grid usually 0.0253 eV, 400 KeV, 14 MeV
 - tabulated 59 incident energies (GEF)
 - with uncertainties !!! on the fitted (to experiments) cumulative yields

- Using NJOY, PREPRO or CALENDF
 - from mf-2 parameters to pointwise data in mf-3
 - from mf-2 parameters in the URR to PT's SSF (Monte Carlo)
 - from mf-5 distributions laws to tabulated
 - from mf-3 to groupwise data
 - from mf-2 parameter to SSF's (Bondarenko)
 - from mf-3, mf-4/mf-5 or mf6 group matrices
- This of course assumes that the evaluator, then the processor are aware of what the reactor physicist needs exactly or can cope with. Usually the latter need to know, but not the first !

Processing steps: three codes

ENDF file

• NJOY12-099

- reconr
- broadr
- unresr
- thermr
- heatr
- gaspr
 - purr
 - acer
 - groupr

ACE file

cross-check



• PREPRO-2017

- **linear**
- **recent**
- **sigma1**
- **sixpack**
- **activate**
- **merger**
- **dictin**
- **groupie**

Processed ENDF file

cross-check



• CALENDF-2010

- calendf
- regroupt
- lecritp
-

PT file

Single script
for an entire
library

- Reactor simulation software, usually proprietary (non exhaustive list)
 - Pin cell, collision probability, lattice codes: WIMS, APOLLO, CASMO, ...
 - Nodal core, MOC (Method of Characteristic): PANTHER, CRONOS, SIMULATE, ...
 - Transmutation: FISPIN, ORIGEN, FISPACT-II,
 - Monte Carlo: MONK, MCNP, TRIPOLI, SERPENT, MC21,
 - Integrated system: VERA (Consortium for Advanced Simulation of LWR), SCALE (ORNL), ERANOS (CEA), ...
 - ...
- None of the above can use non-processed, raw nuclear data, so they all rely in parts or in all on the data form(s) outputted by one or more of the processing codes

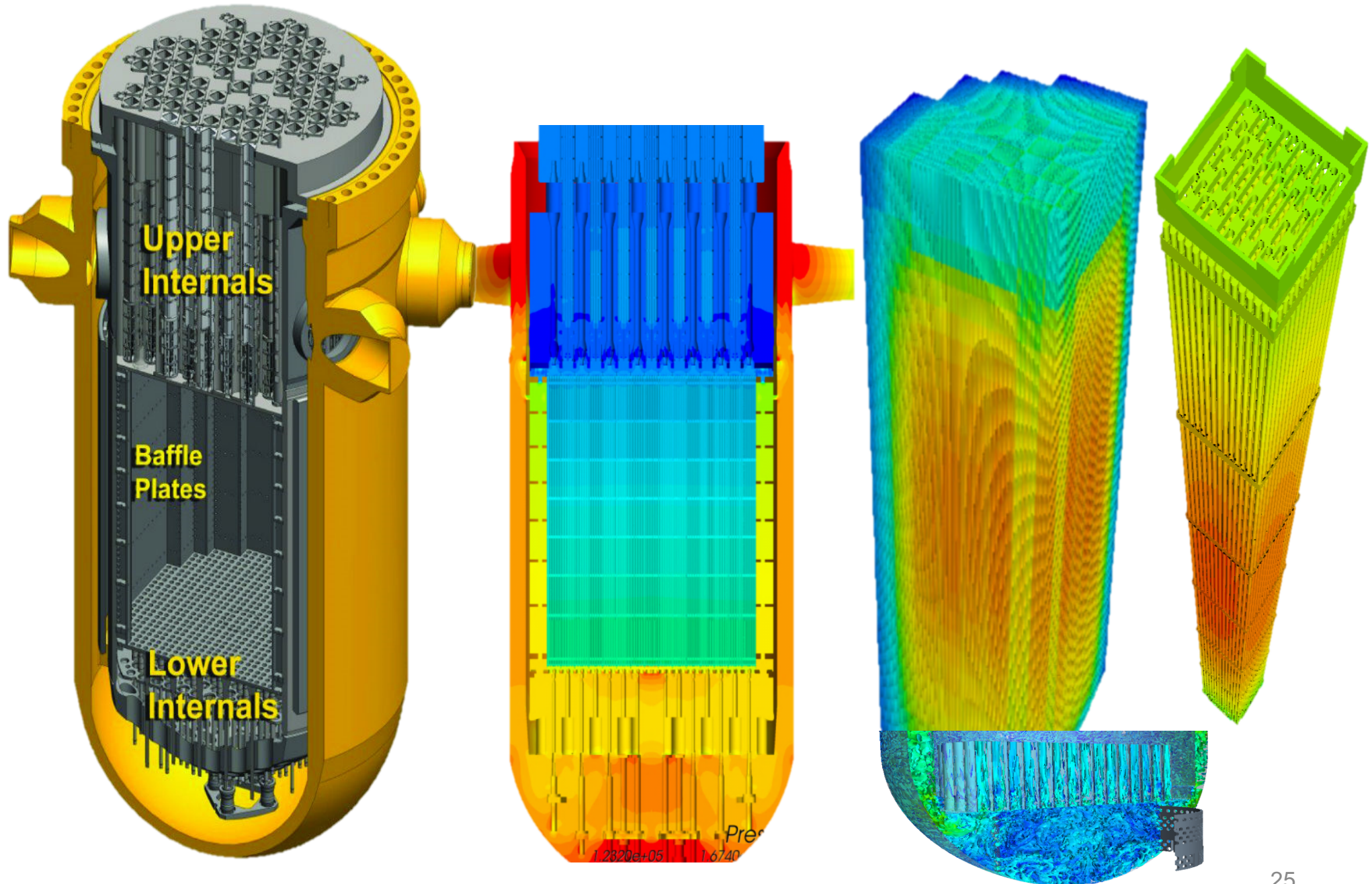


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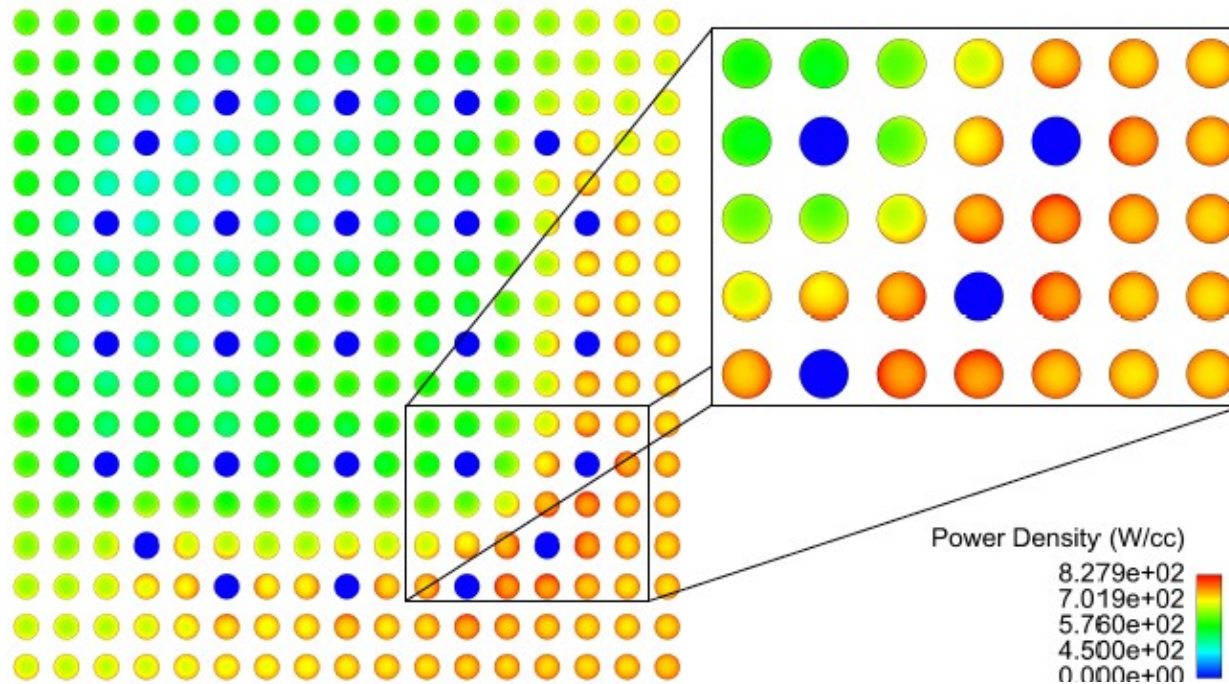
Reactor, pile criticality issues



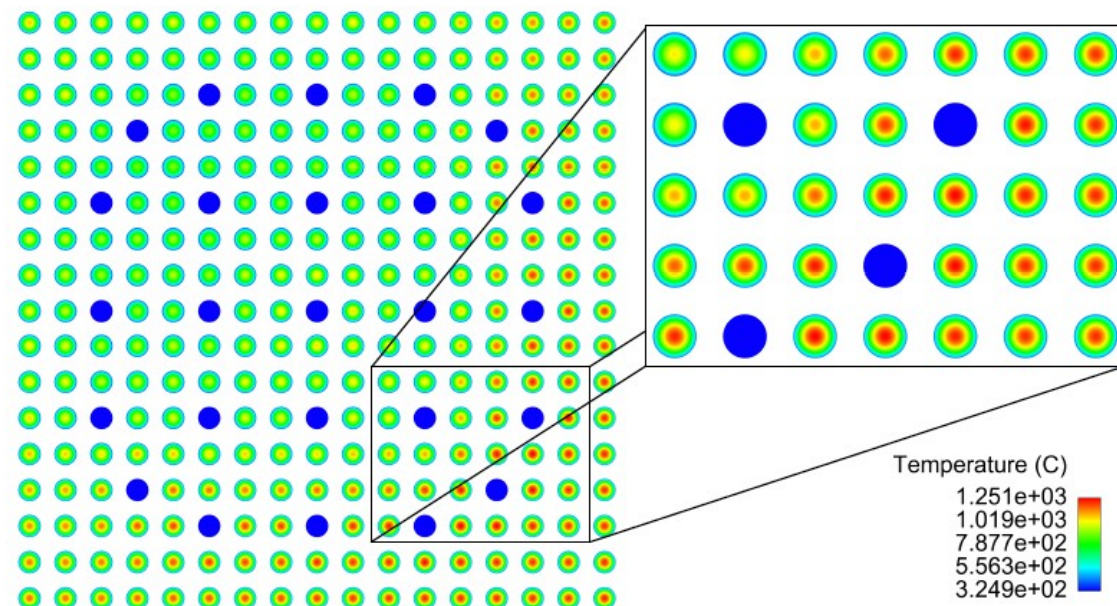


High-Resolution Reactor Core Simulations

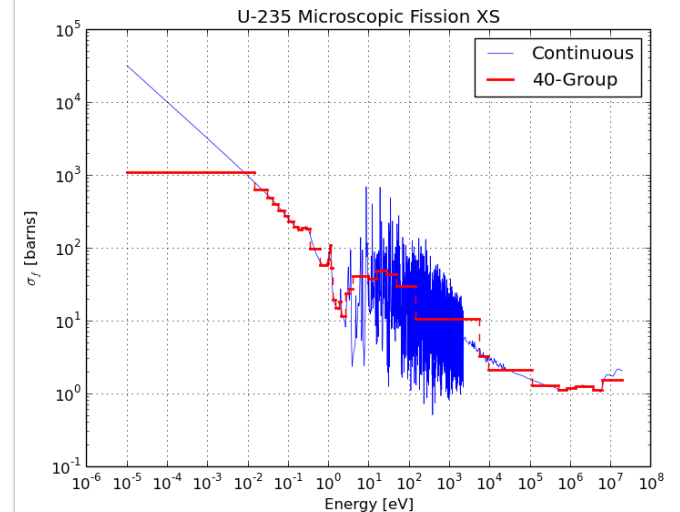
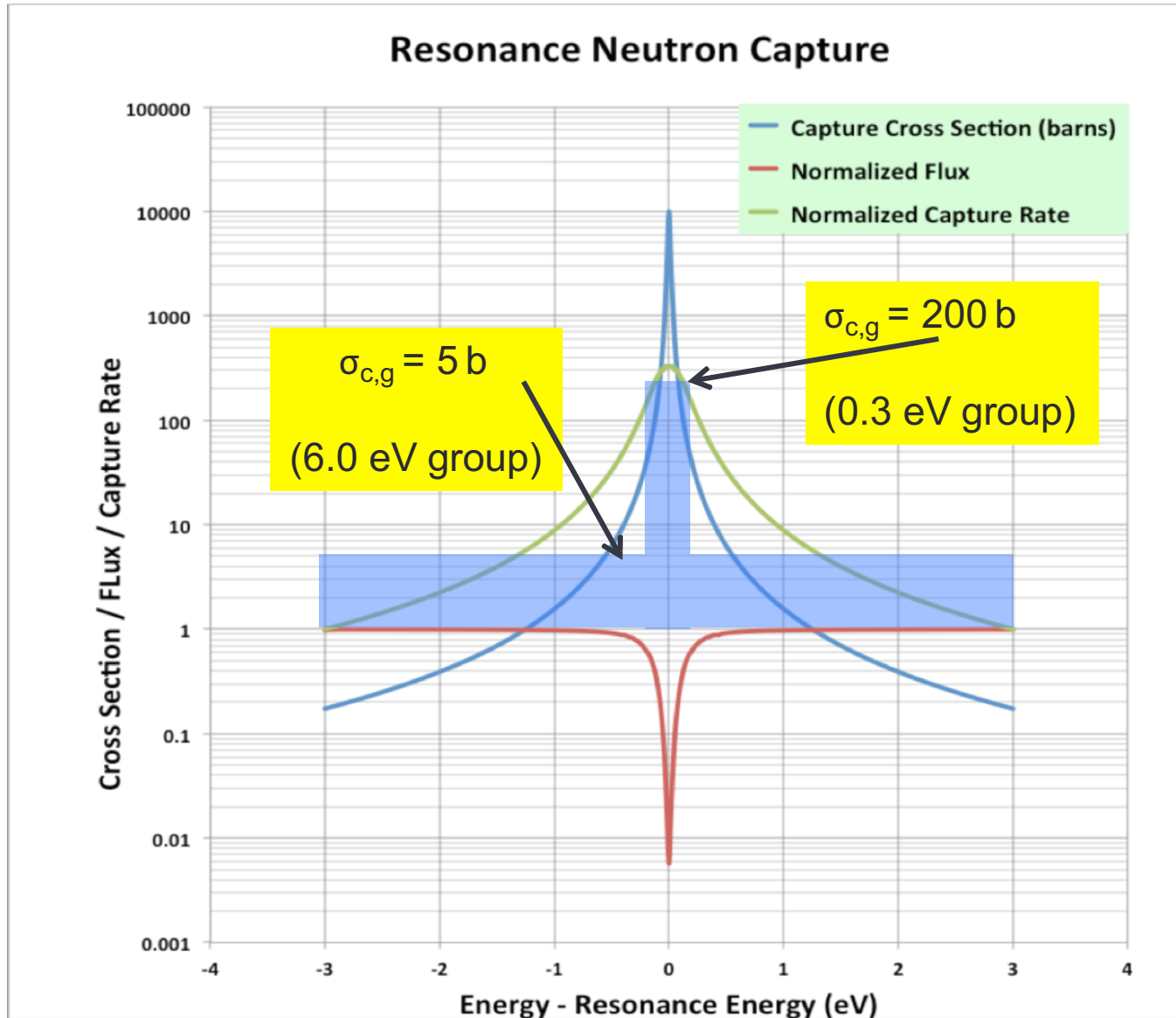
Radial Fission Rates
and
Fuel Temperatures



*High-resolution
requires full
local detail*



200 pcm jungle: multi-group resonance XS



$$\sigma_{c,g} \equiv \frac{\int_E^{E_g} \sigma_c(E) \phi(E) dE}{\int_E^{E_g} \phi(E) dE}$$

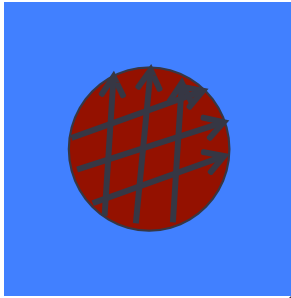
$$\phi_g^{N.R.} = \frac{(\sigma_{pot,f} + \sigma_e)}{\sigma_{c,g} + (\sigma_{pot,f} + \sigma_e)}$$

$$\phi_g^{N.R.} \cong \frac{75b}{\sigma_{c,g} + 75b}$$

As group width increases, resonance absorption has smaller impact on multi-group flux



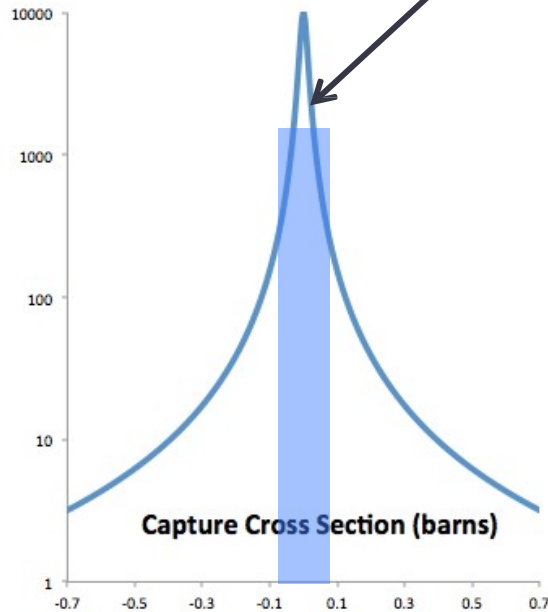
Equivalence for multi-group XS



$$\int_{E_{g-1}}^{E_g} \Sigma(E) \phi^{MC}(E) dE = \Sigma_g \phi_g^{MC} \neq \Sigma_g \bar{\phi}_g^{Multi-group}$$

$$\int_{E_{g-1}}^{E_g} e^{-\Sigma(E)\tau/\beta} dE \neq e^{-\Sigma_g \tau/\beta} \int_{E_{g-1}}^{E_g} dE$$

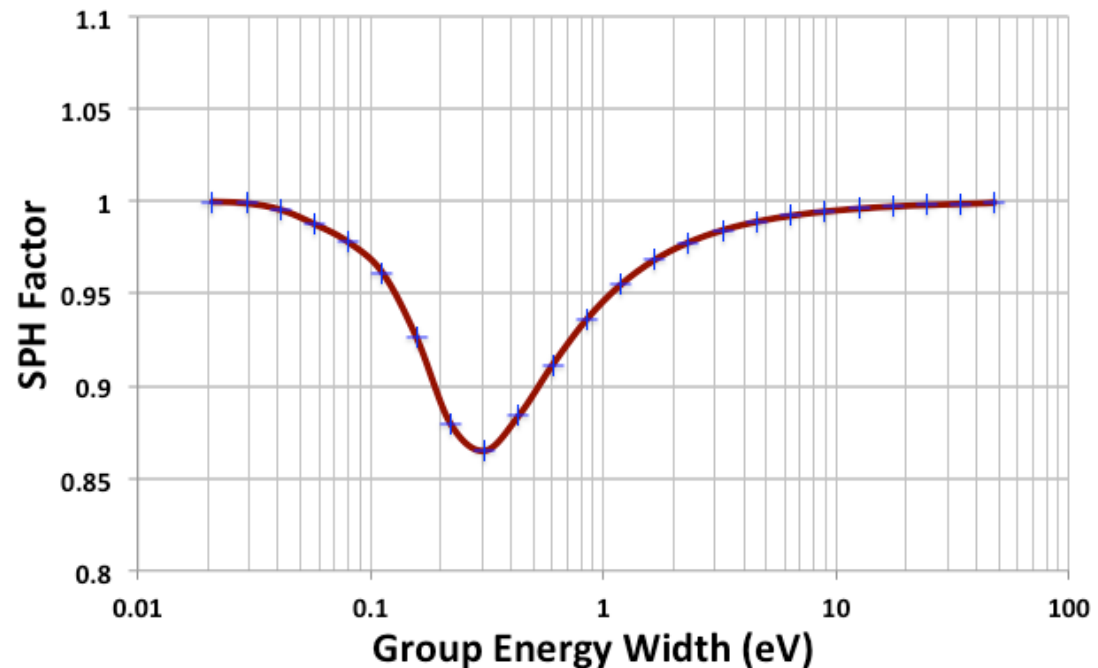
$$\int_{E_{g-1}}^{E_g} e^{-\Sigma(E)\tau/\beta} dE \equiv e^{-\overset{SPH}{\Sigma_g} \tau/\beta} \int_{E_{g-1}}^{E_g} dE$$



$$\hat{\Sigma}_g \equiv SPH \cdot \Sigma_g$$

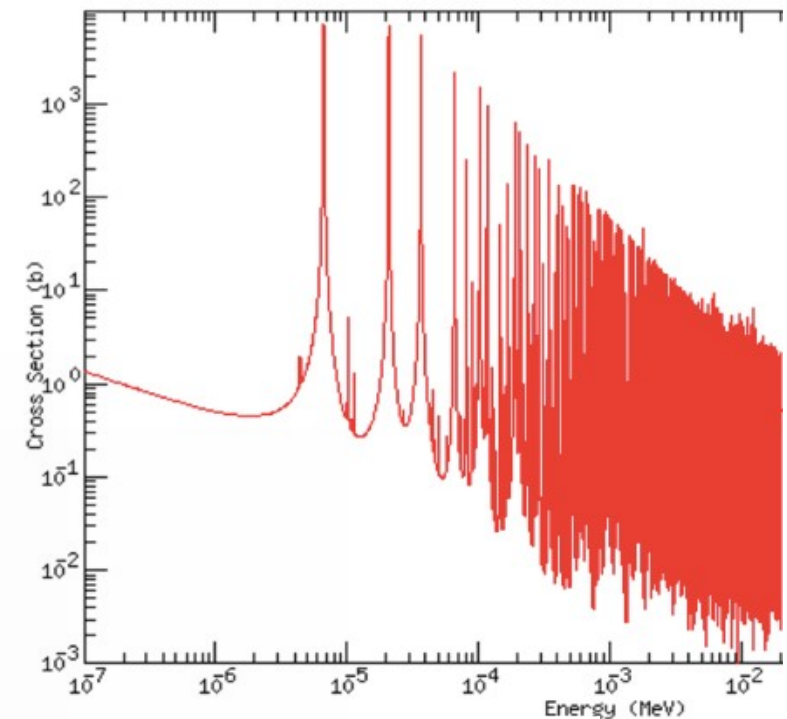
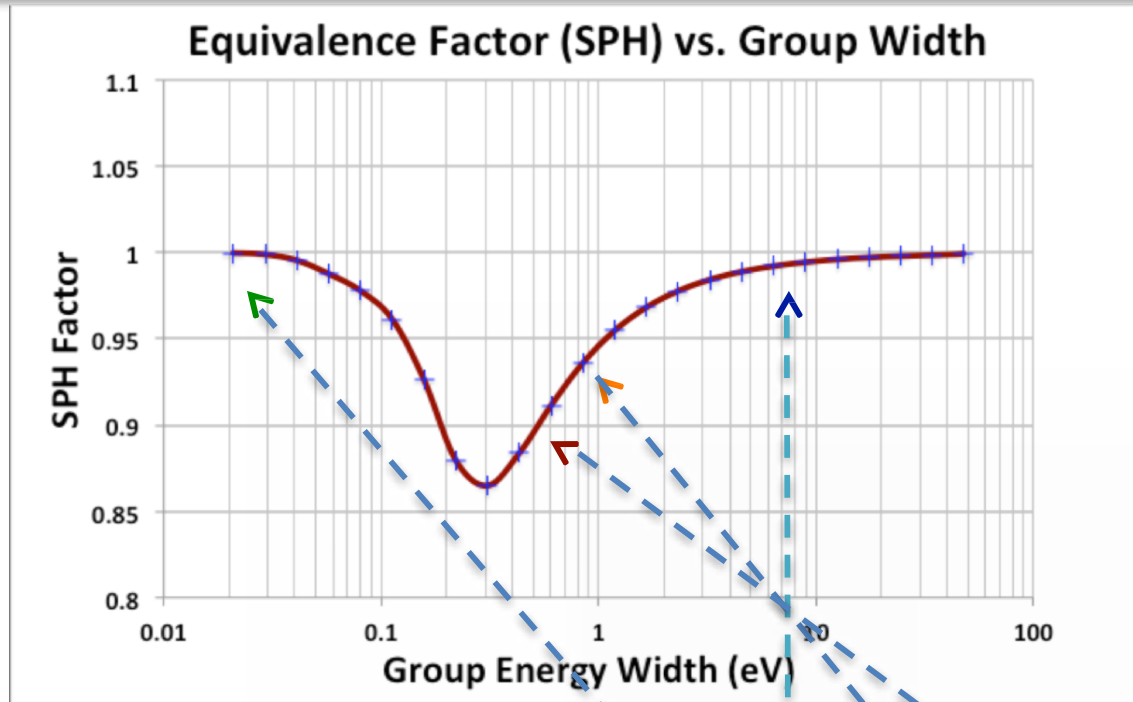
$$\Sigma_g \phi_g^{MC} = \hat{\Sigma}_g \bar{\phi}_g^{Multi-group}$$

Equivalence Factor (SPH) vs. Group Width





Selecting Multi-Group Energy Boundaries



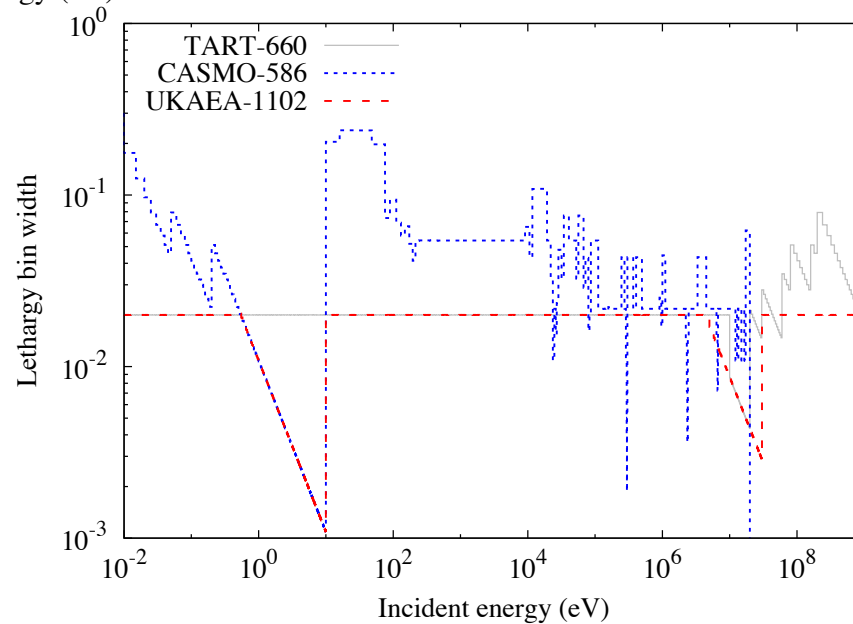
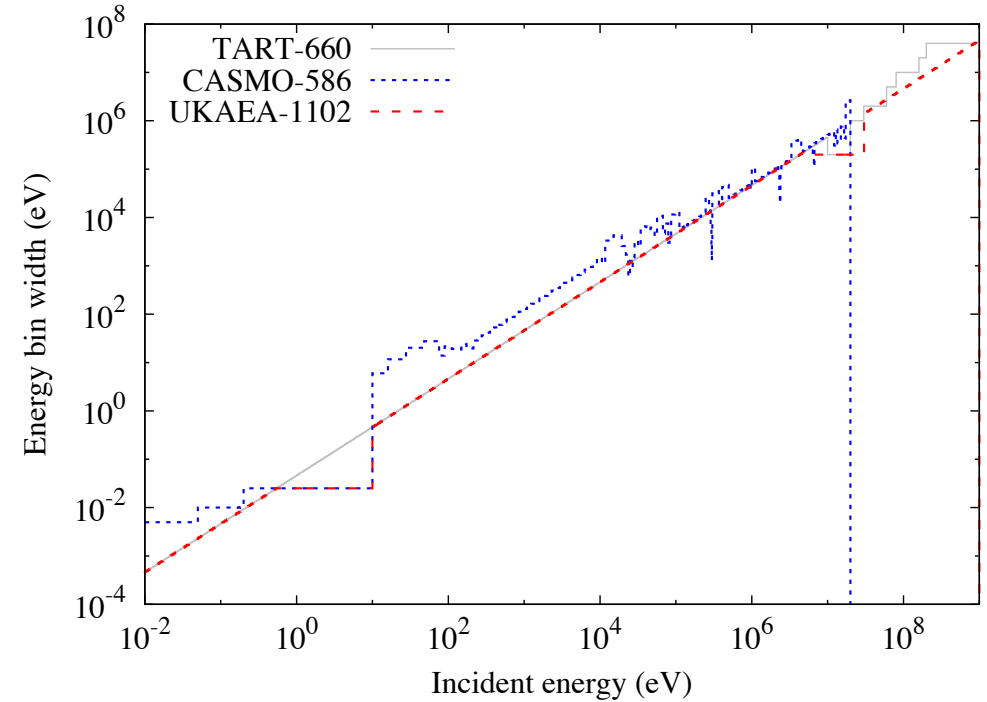
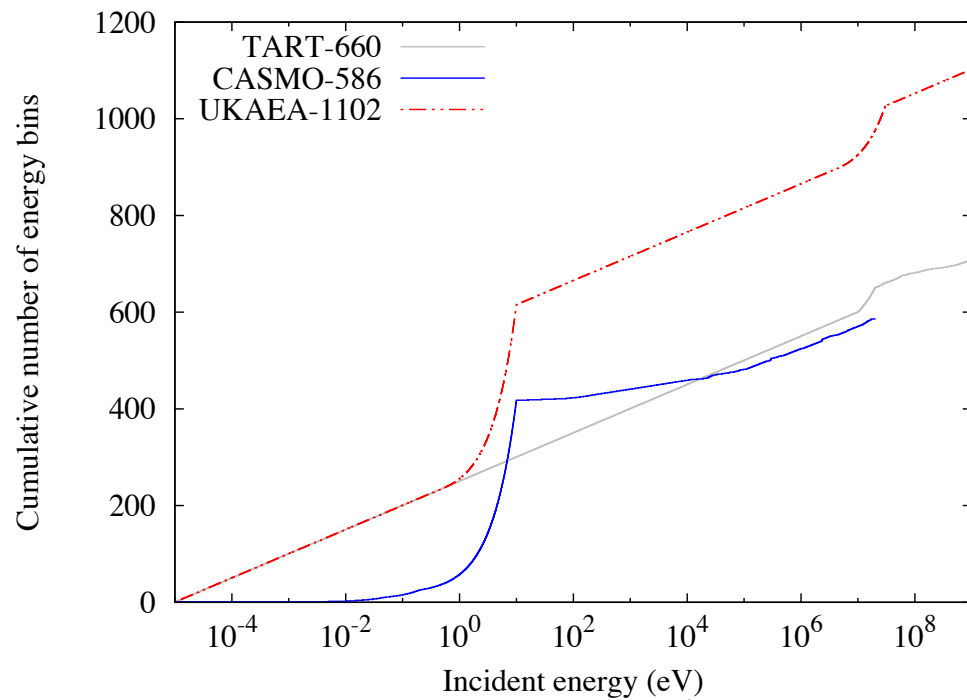
U-238 res.	Energy group width (eV) near resonance peak			
Energy eV	WIMS-69	SHEM-361	Xmas-172	CASL-51
36.68	10.30	~0.05	3.50	18.30
20.87	11.70	~0.01	3.15	16.60
6.67	5.90	~0.01	0.8 - 1.4	0.3 – 0.8

1000's of energy groups are needed to blindly overcome group boundary sensitivities

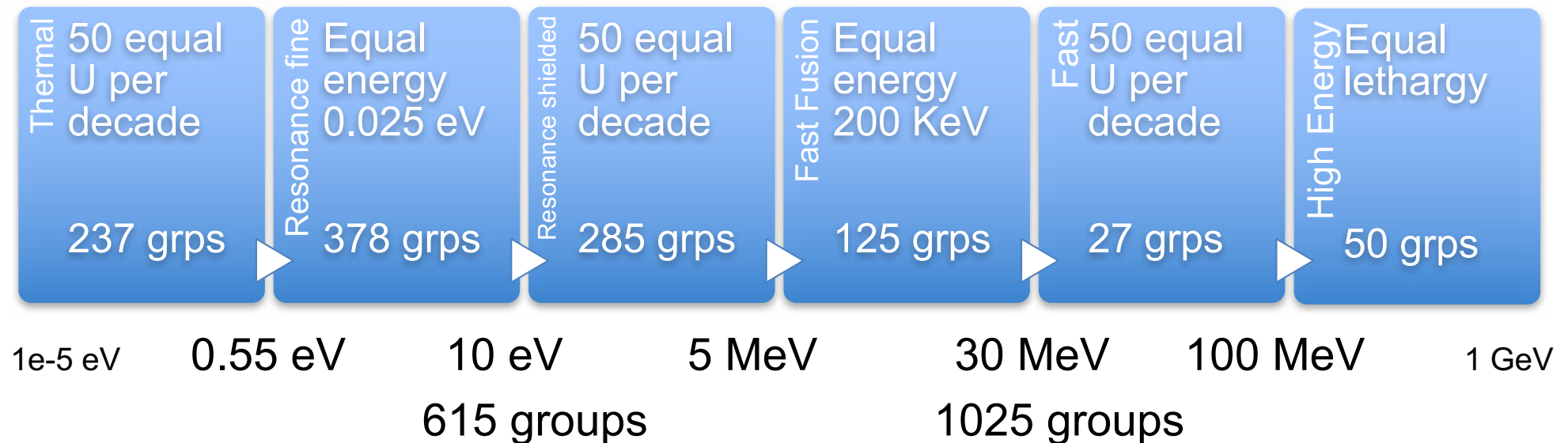
Intermediate group widths produce results that are sensitive to “equivalence factors”



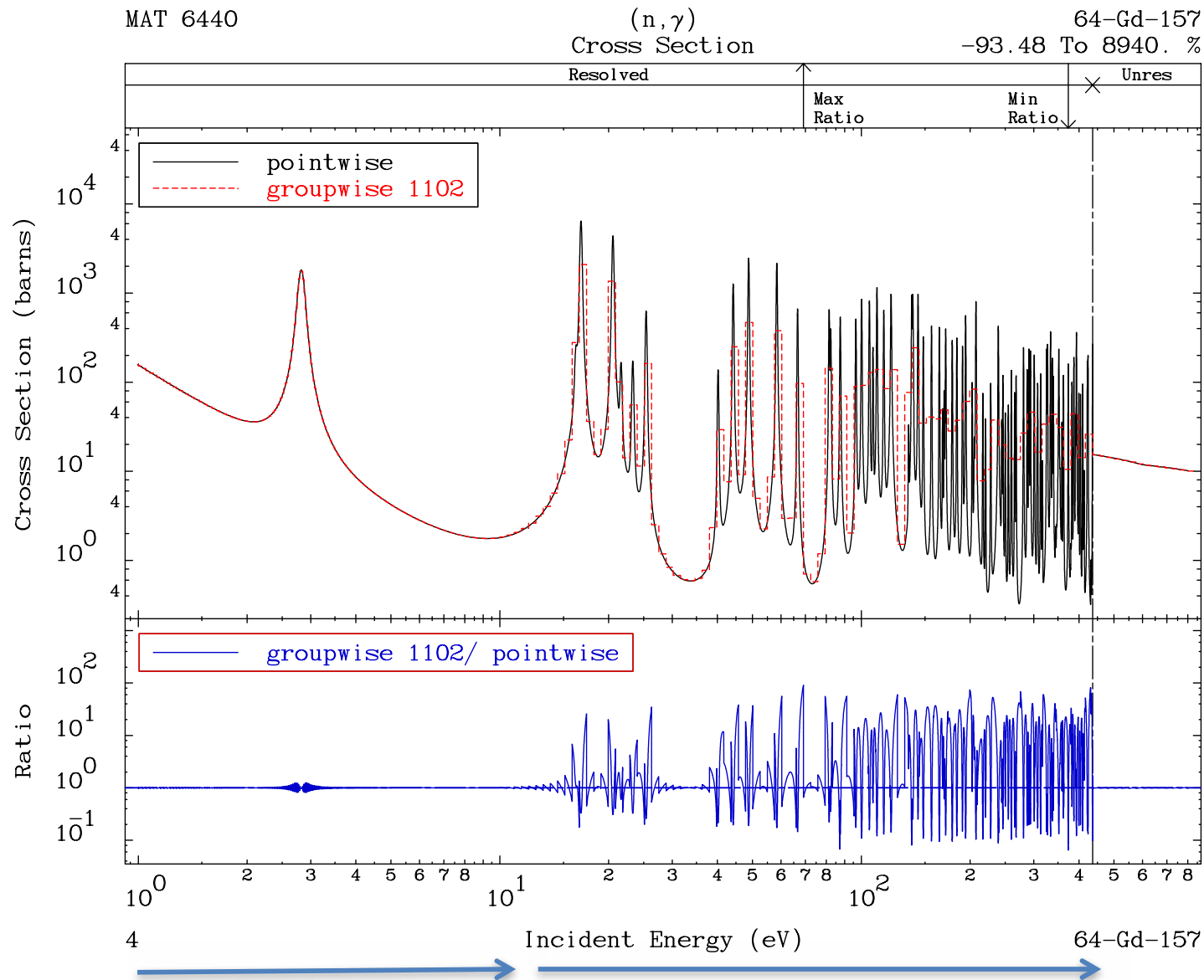
Group structures 586 to 1000+



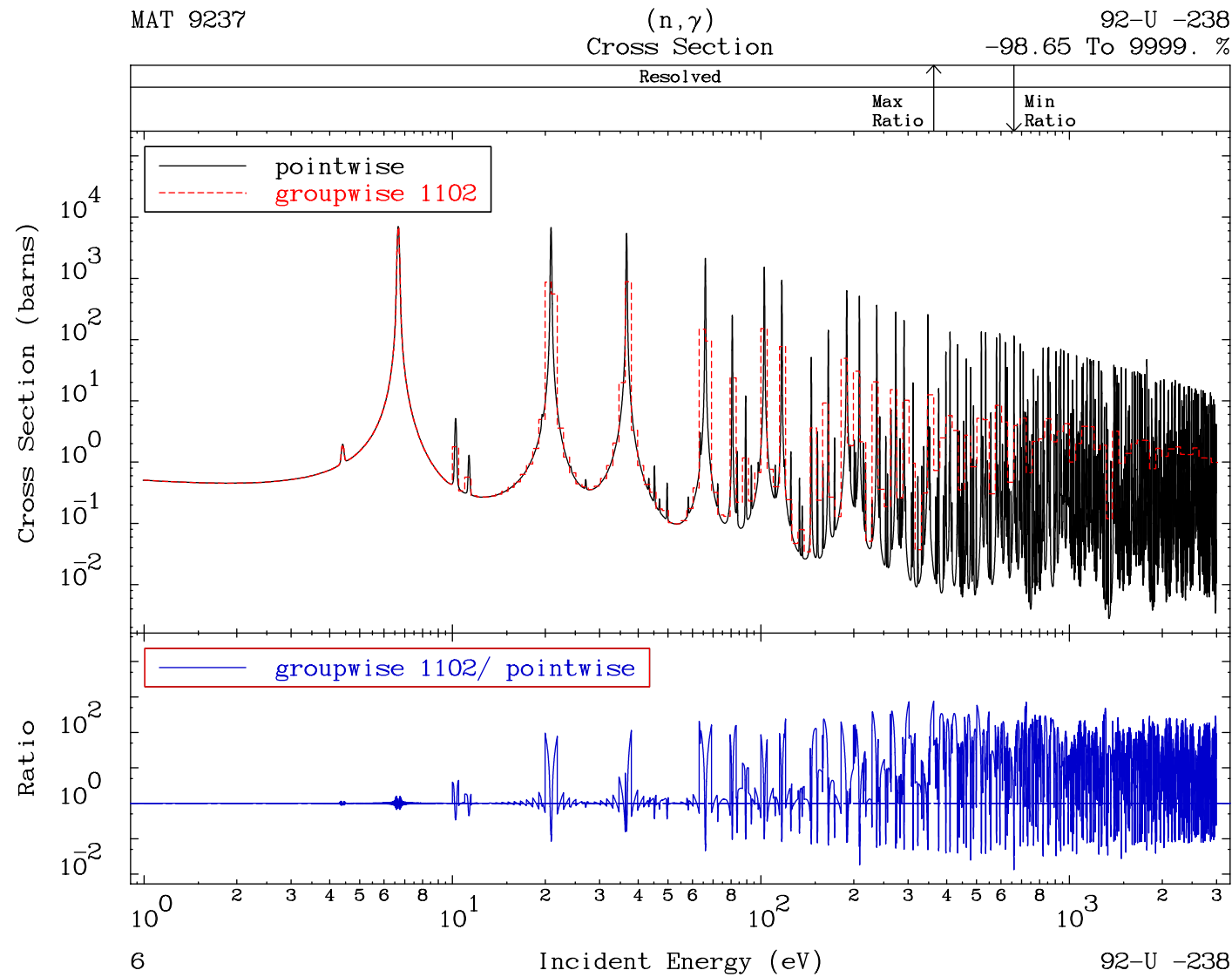
- For all target nuclides
- 1102 energy groups for all applications alike



- 378 fine groups in the resonance range
- Resonance shielded data available in the RRR (0.1 eV) up to the end of the URR for all nuclides IDs
- Fast fine structure for accurate threshold XS reaction rate



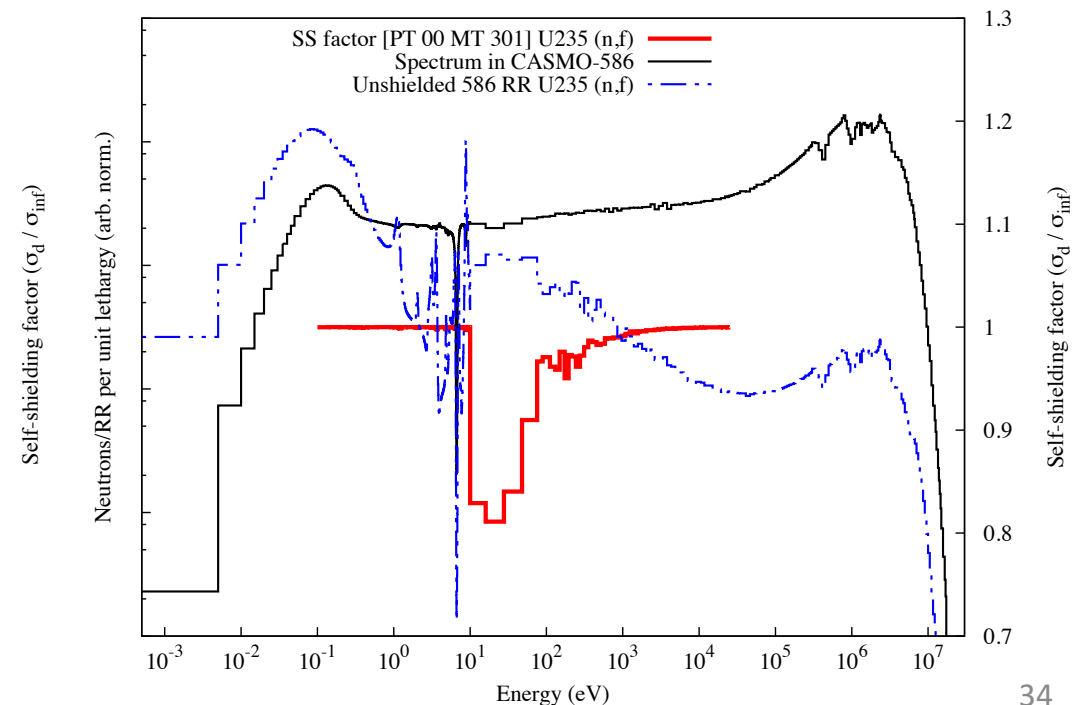
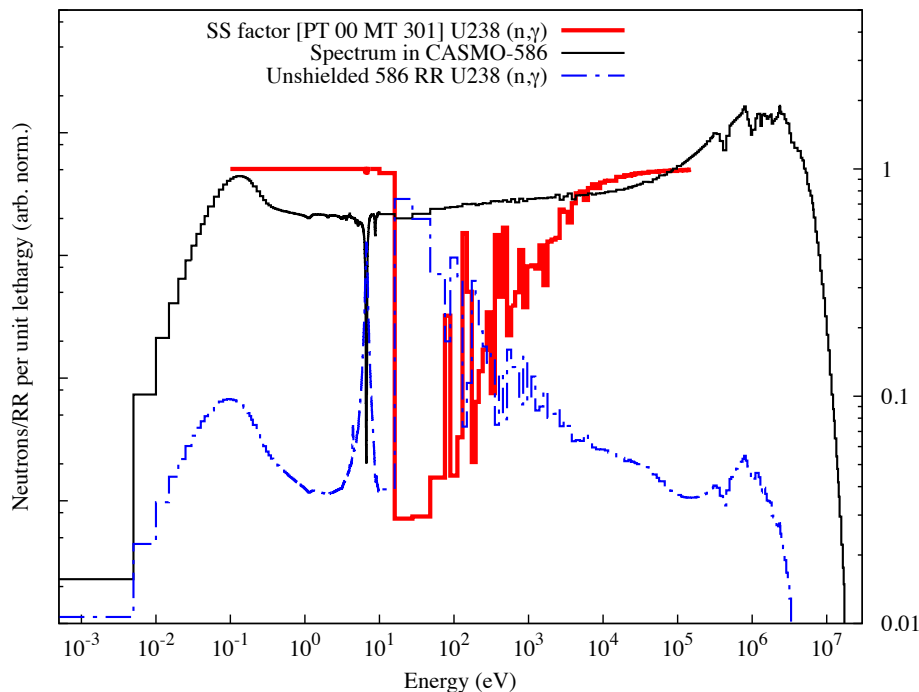
Fine group to 10 eV Resonance shielded to end of URR



Fine group to 10 eV → Resonance shielded to end of URR

- 586 gprs CASMO data for ENDF/B-VII.1, with CALENDF PTs for self-shielding. Applied to major actinides
- **Left:** U8 capture RR and SSFs **Right:** U5 fission RR+SSFs

Note: 586 gprs treatment of <10 eV requires no SSFs! No so for >10 eV, where significant SS occurs and must be accounted for.



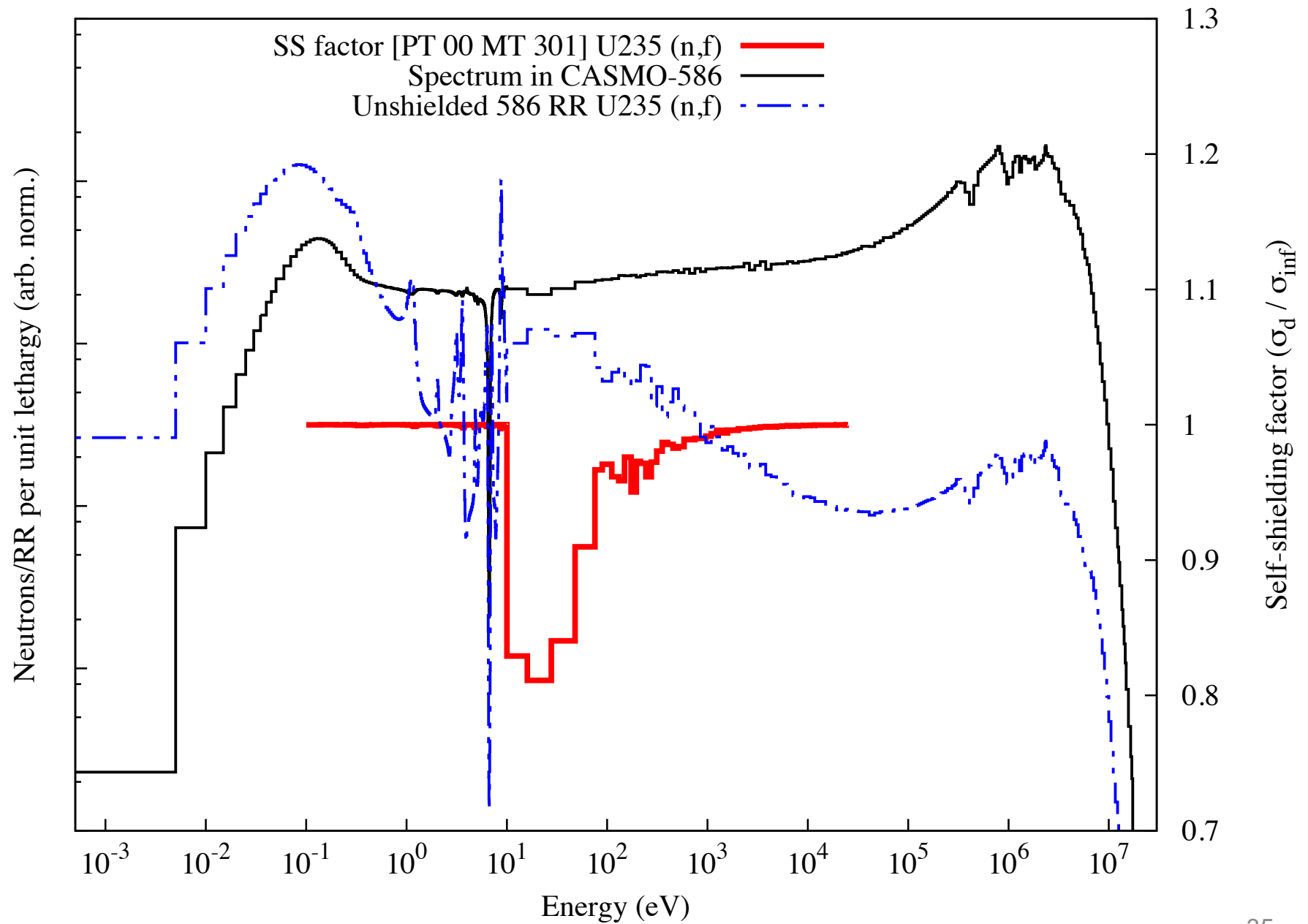


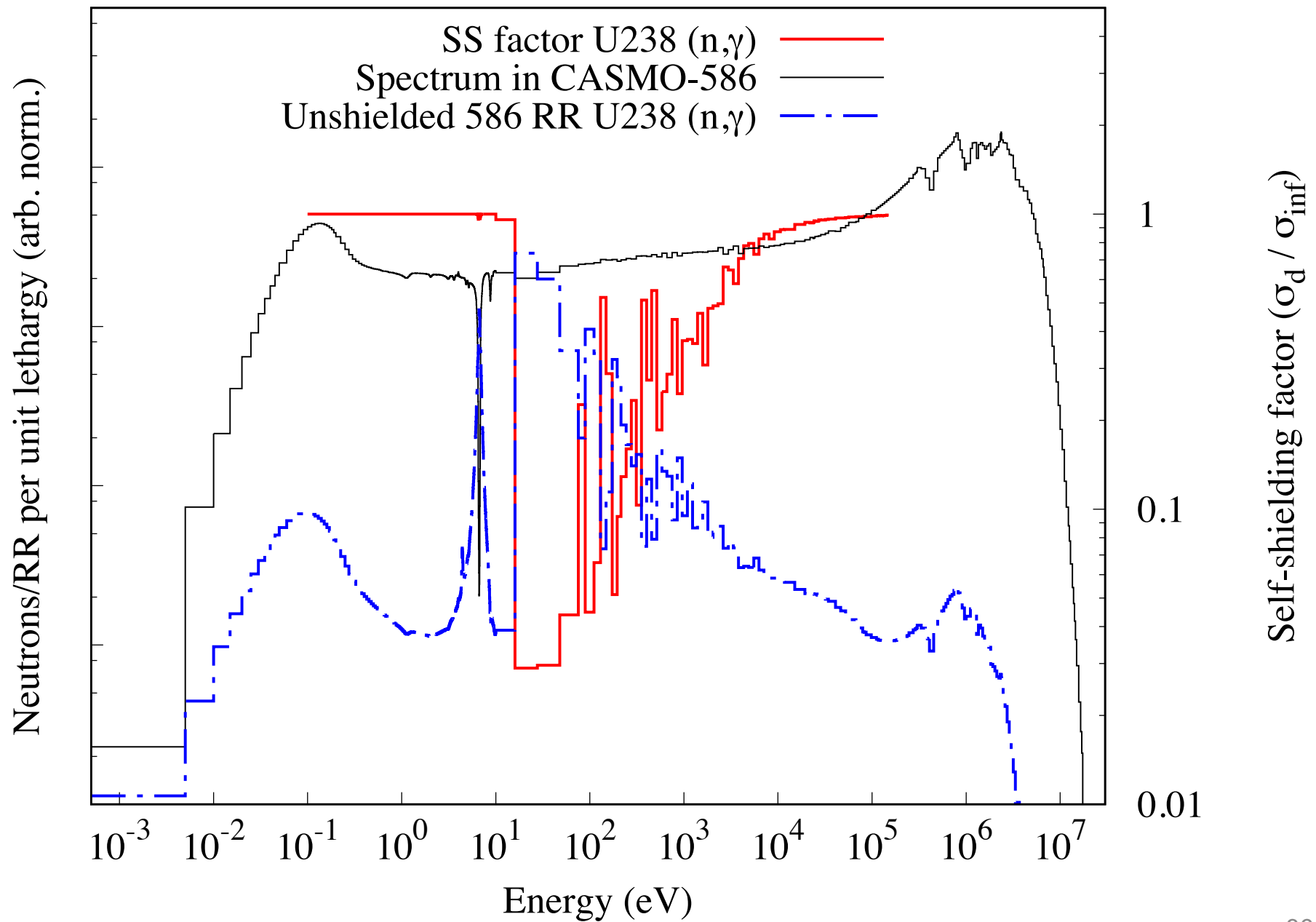
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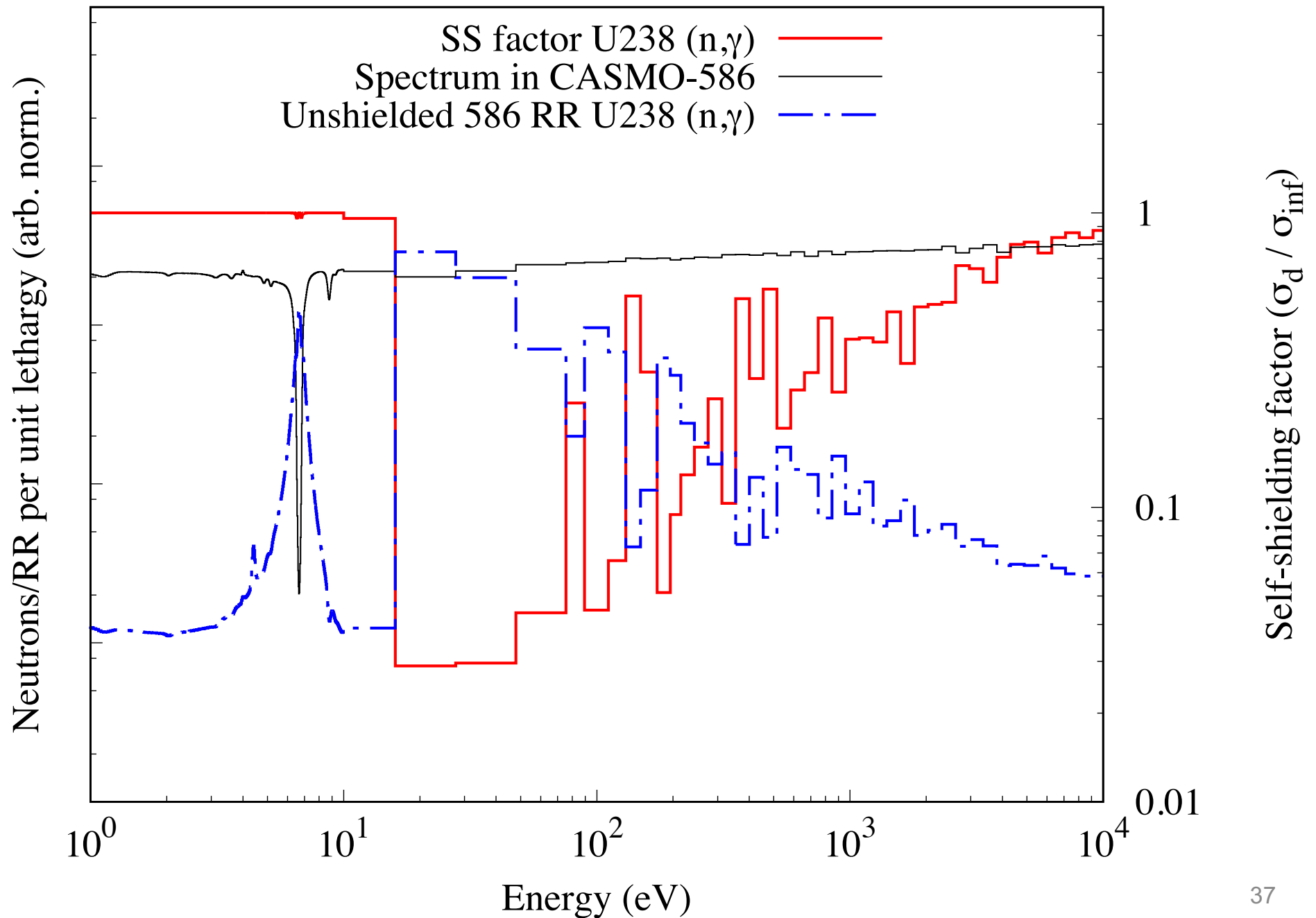
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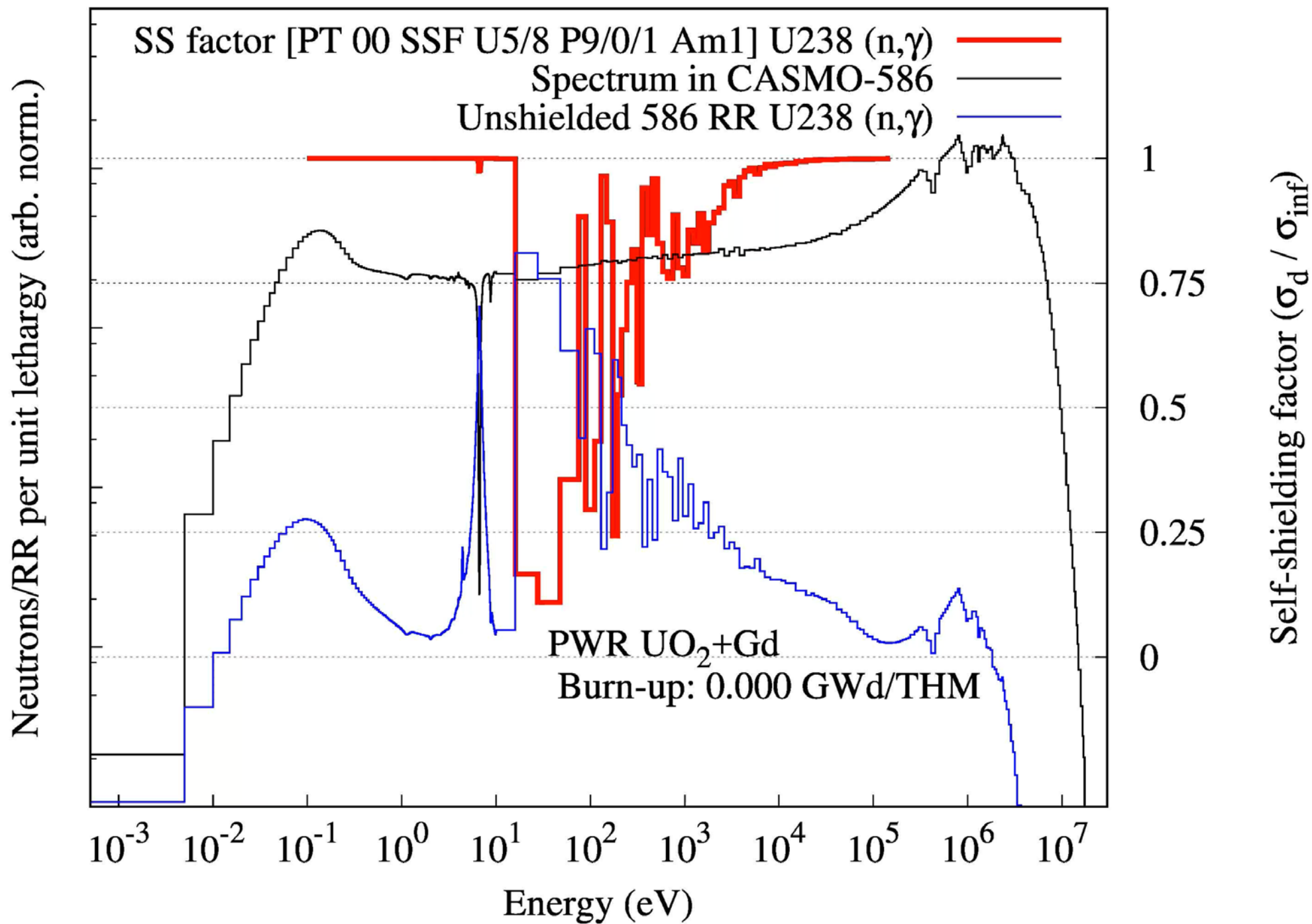
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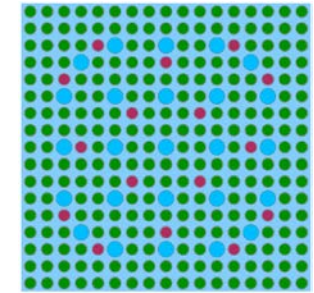
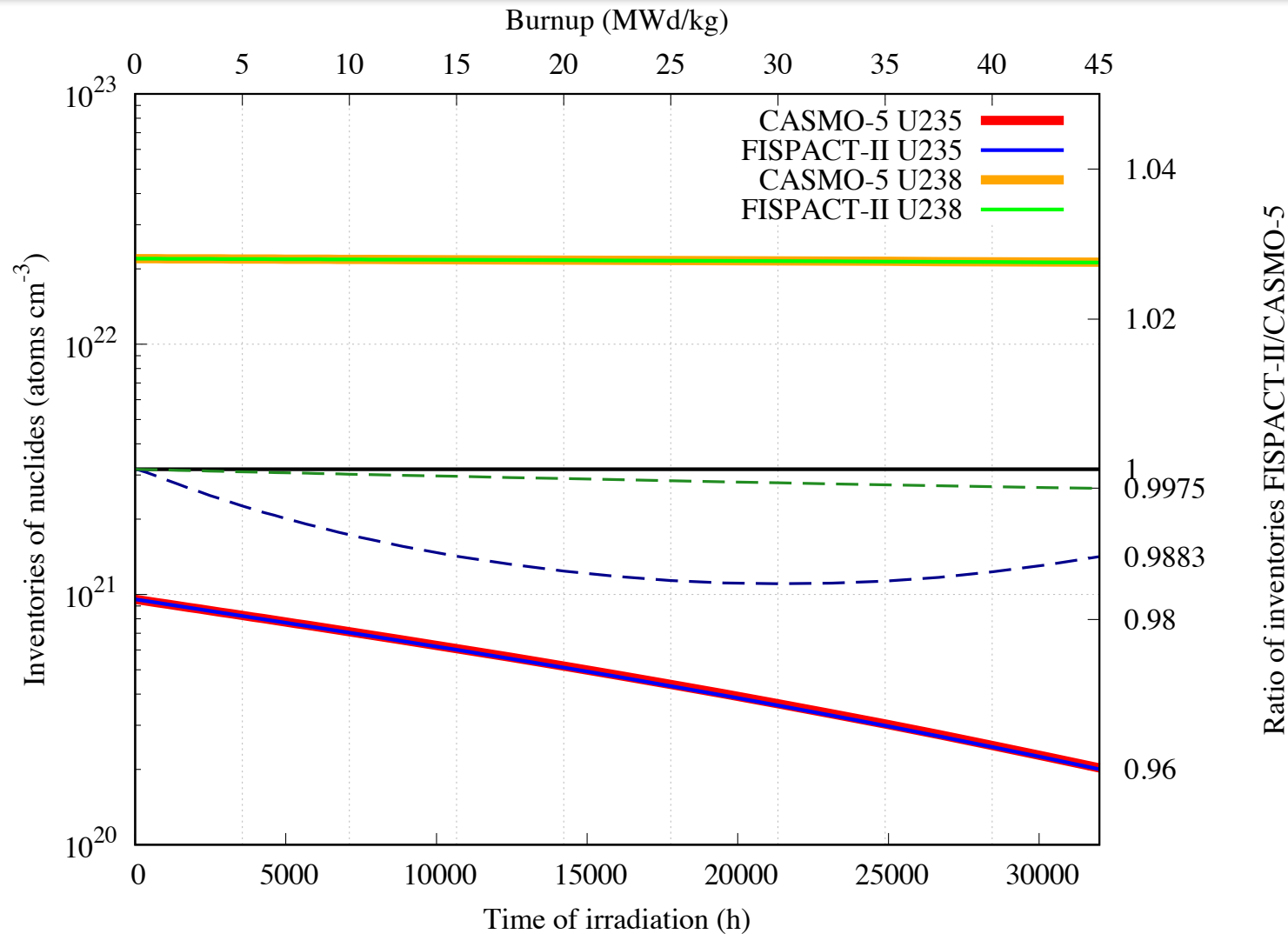
U²³⁵ fission











Takahama-3

Takahama-3 assembly uranium inventories from CASMO-5 and FISPACT-II simulations over a 45 GWd/THM simulation. Ton of Heavy Metal
The ratio of ²³⁵U (ending at 1.2% difference) and ²³⁸U (ending at 0.25% difference) are also shown.

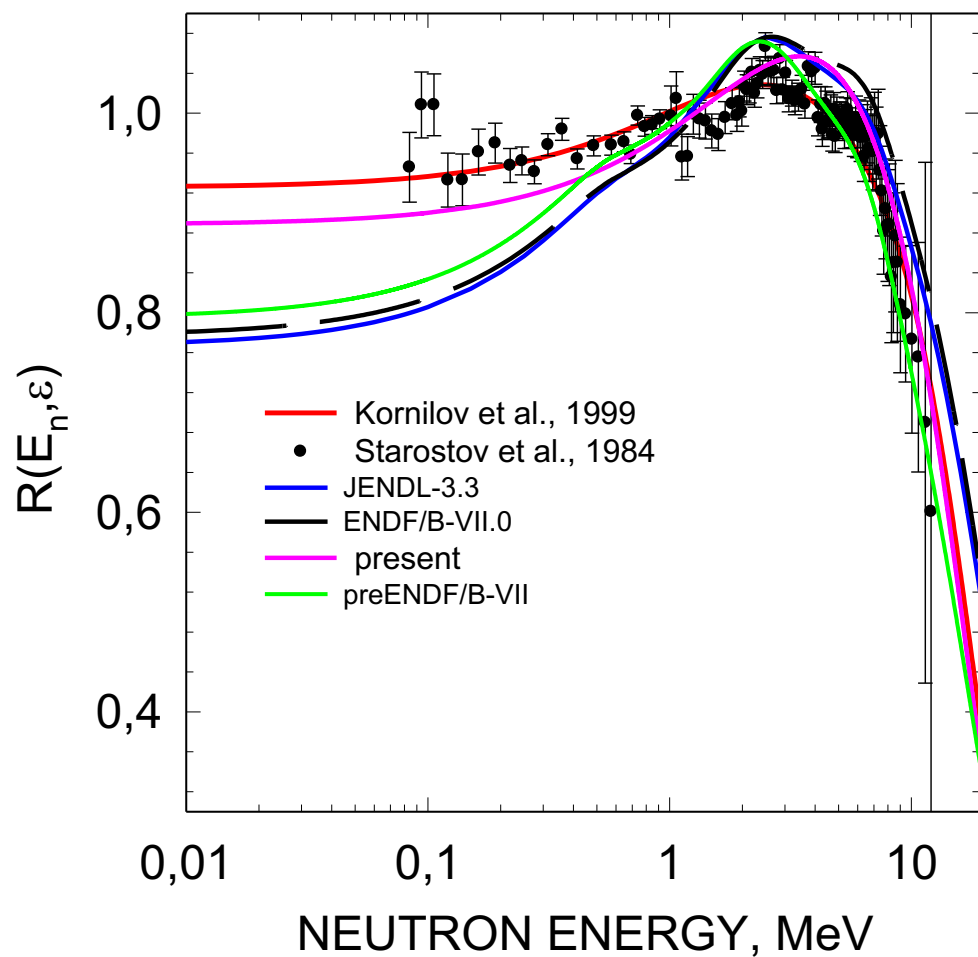
- Are emitted particle spectra important for LWR ?
 - energy dependence, E_n
 - energy profile

Let us look at fission, but think also inelastic,...

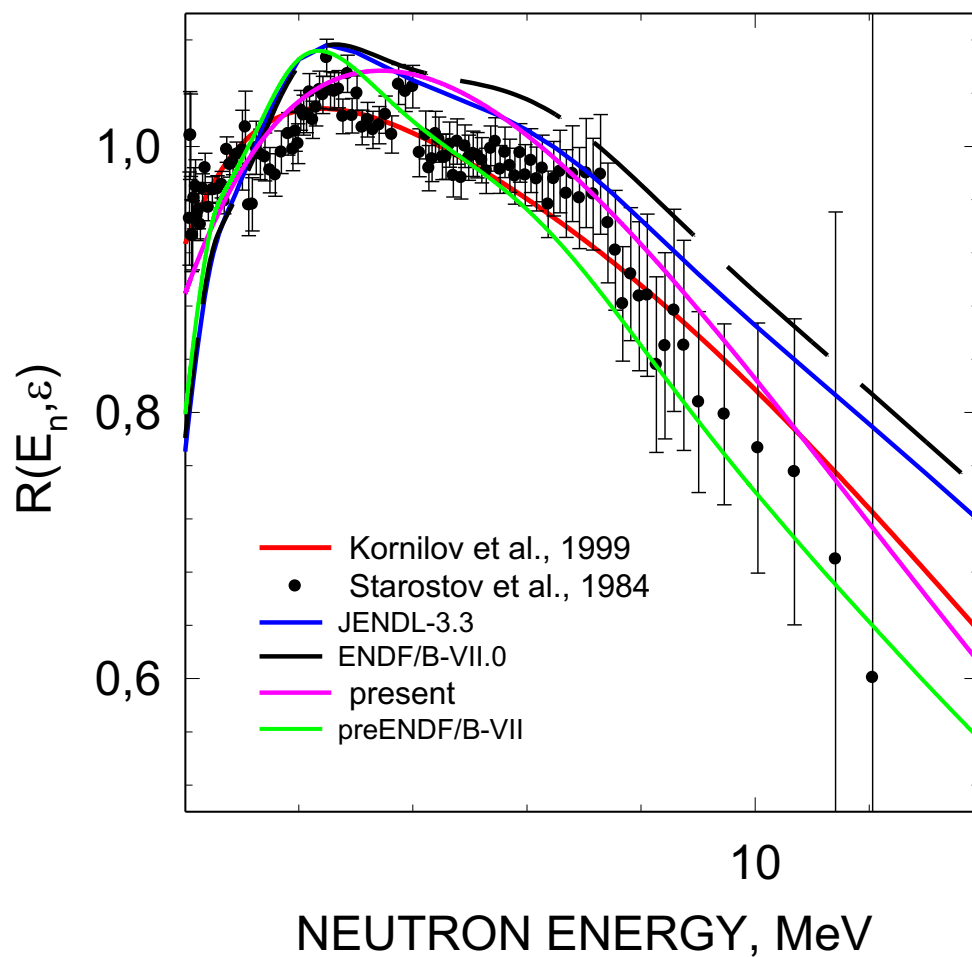
- Single MF-5 MT-18 !! and a tuned thermal nu..
- MF-5 have been better evaluated over the years and we look at the impact on well established ICSBEP benchmarks with the Monte Carlo code TRIPOLI



^{235}U FISSION NEUTRON SPECTRUM
 $E_n \sim E_{th}$



^{235}U FISSION NEUTRON SPECTRUM
 $E_n \sim E_{th}$





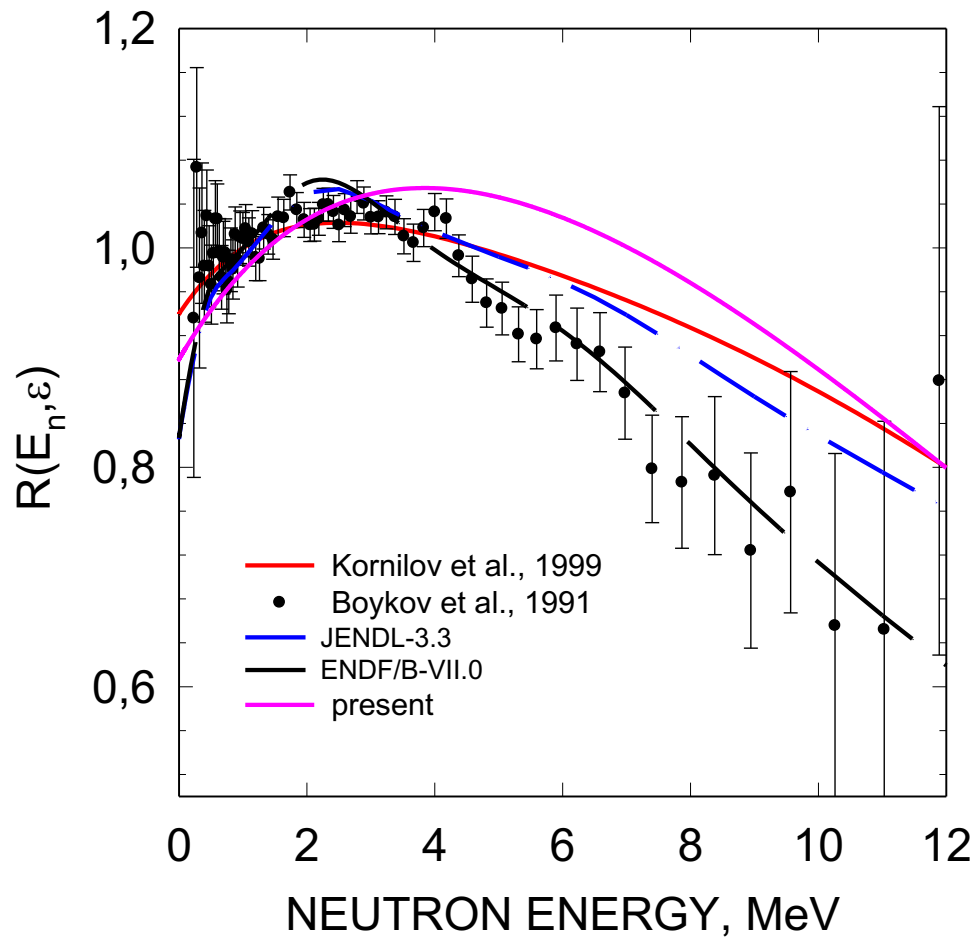
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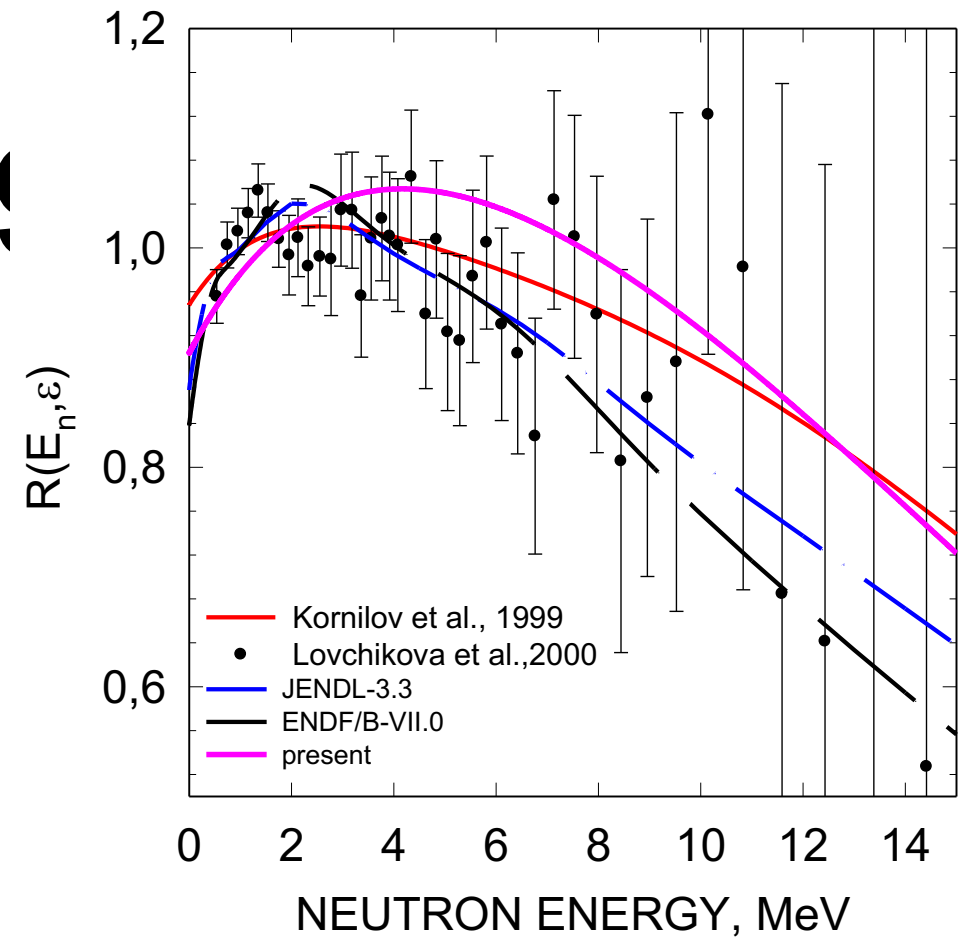
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 ^{235}U PNFS

^{235}U FISSION NEUTRON SPECTRUM
 $E_n \sim 2.9\text{MeV}$

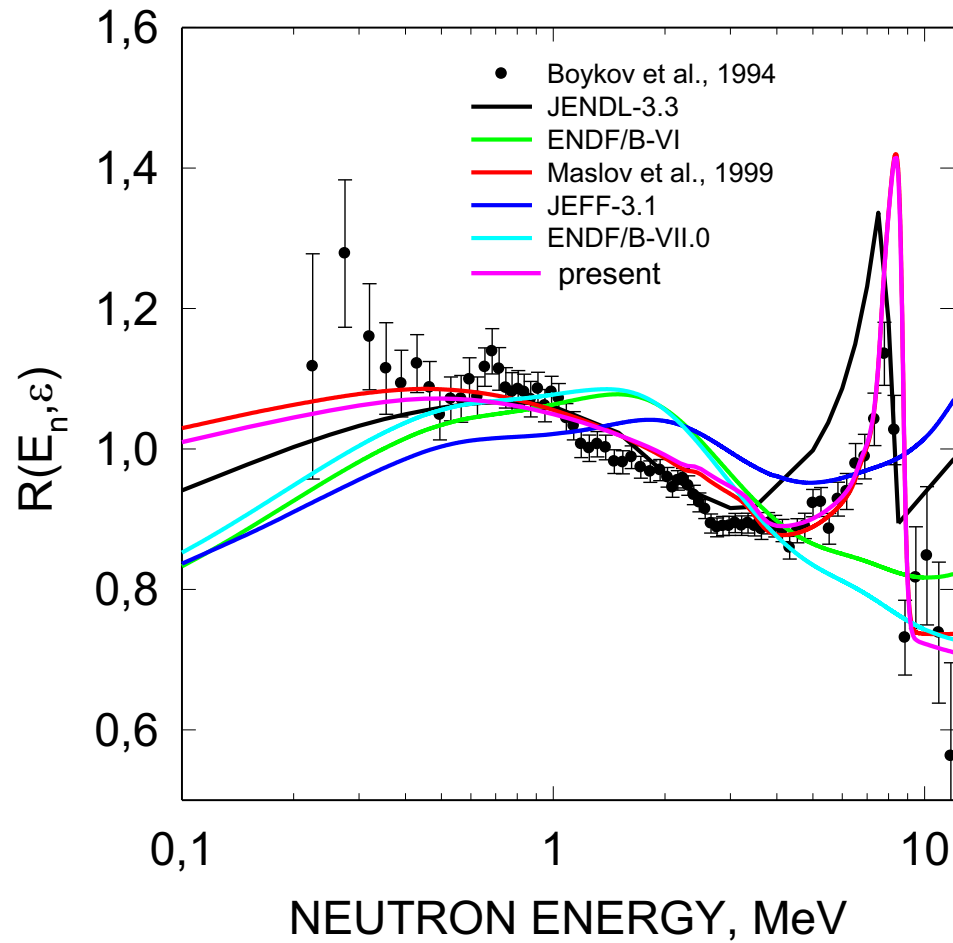


^{235}U FISSION NEUTRON SPECTRUM
 $E_n \sim 5\text{MeV}$

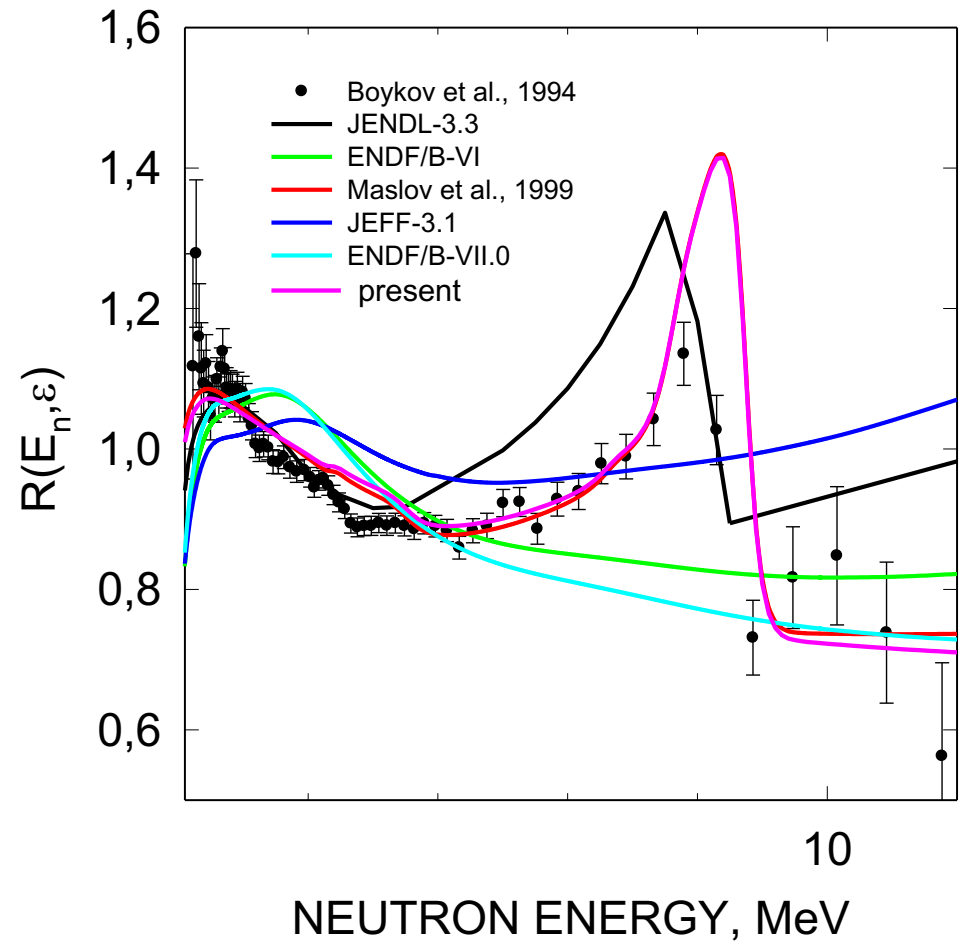




^{235}U PROMPT FISSION NEUTRON
SPECTRUM, $E_n=14.7$ MeV

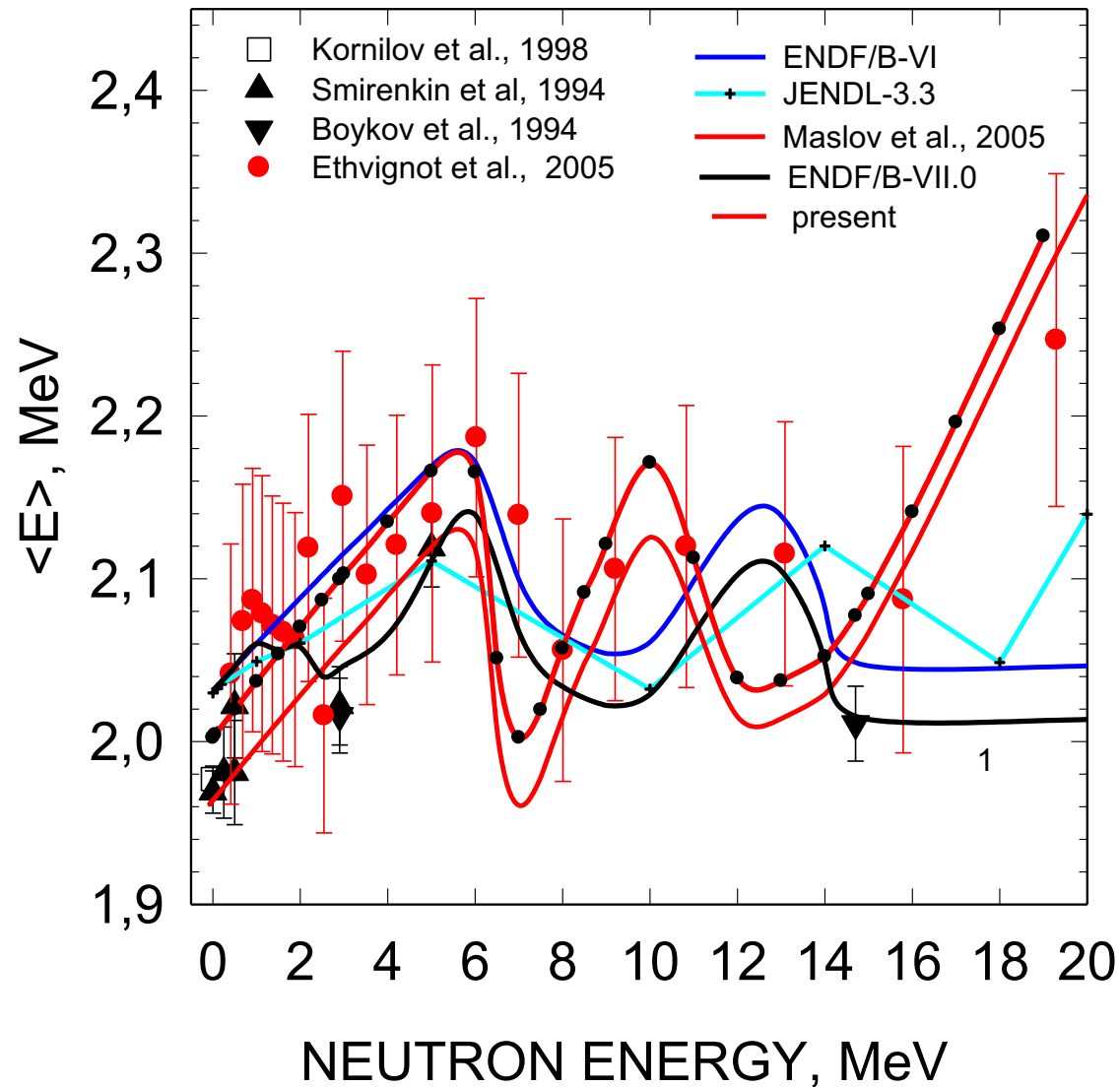


^{235}U PROMPT FISSION NEUTRON
SPECTRUM, $E_n=14.7$ MeV



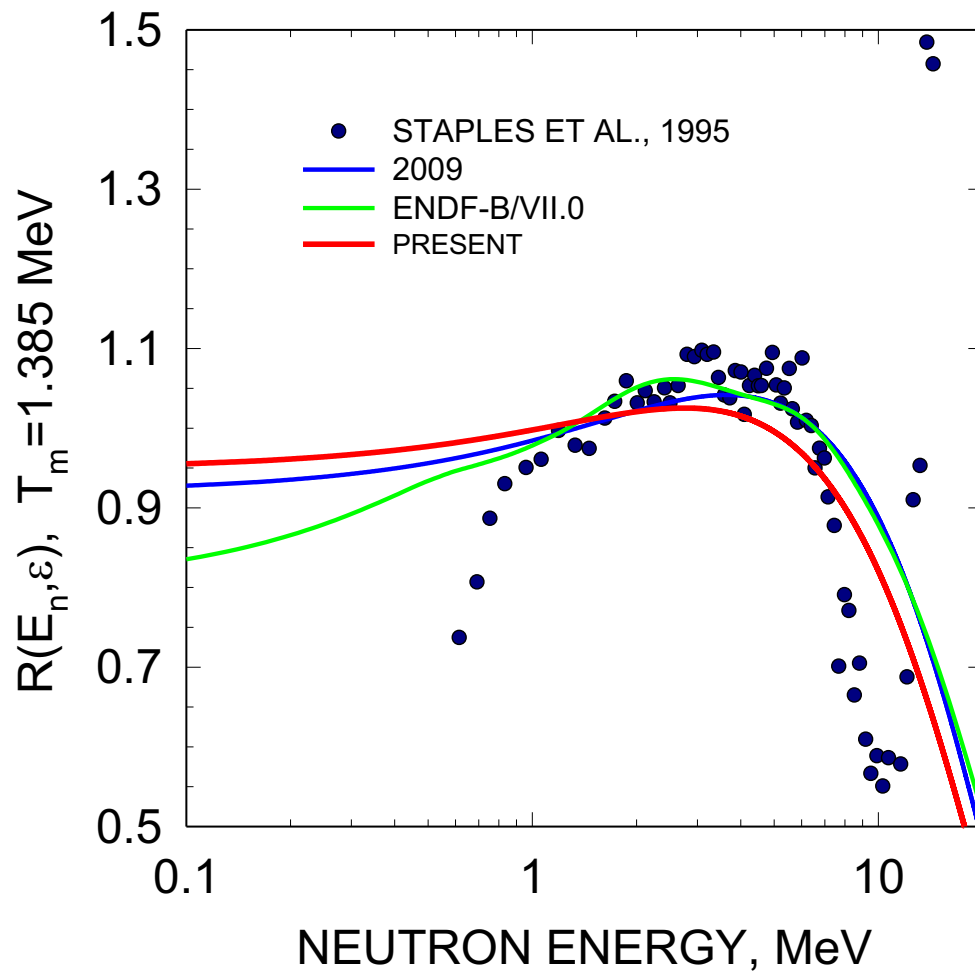


^{235}U : AVERAGE ENERGY OF PFNS

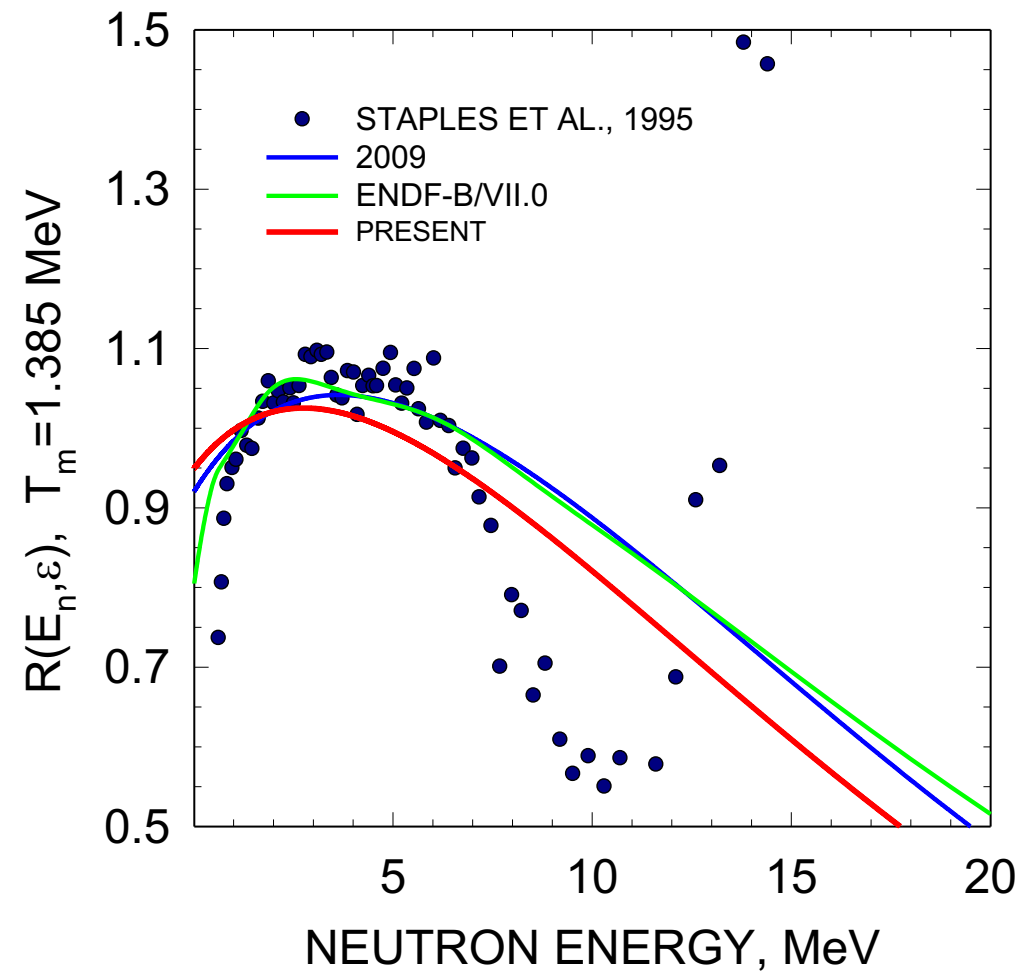




^{239}Pu FISSION NEUTRON SPECTRUM
 $E_n \sim 0.5 \text{ MeV}$

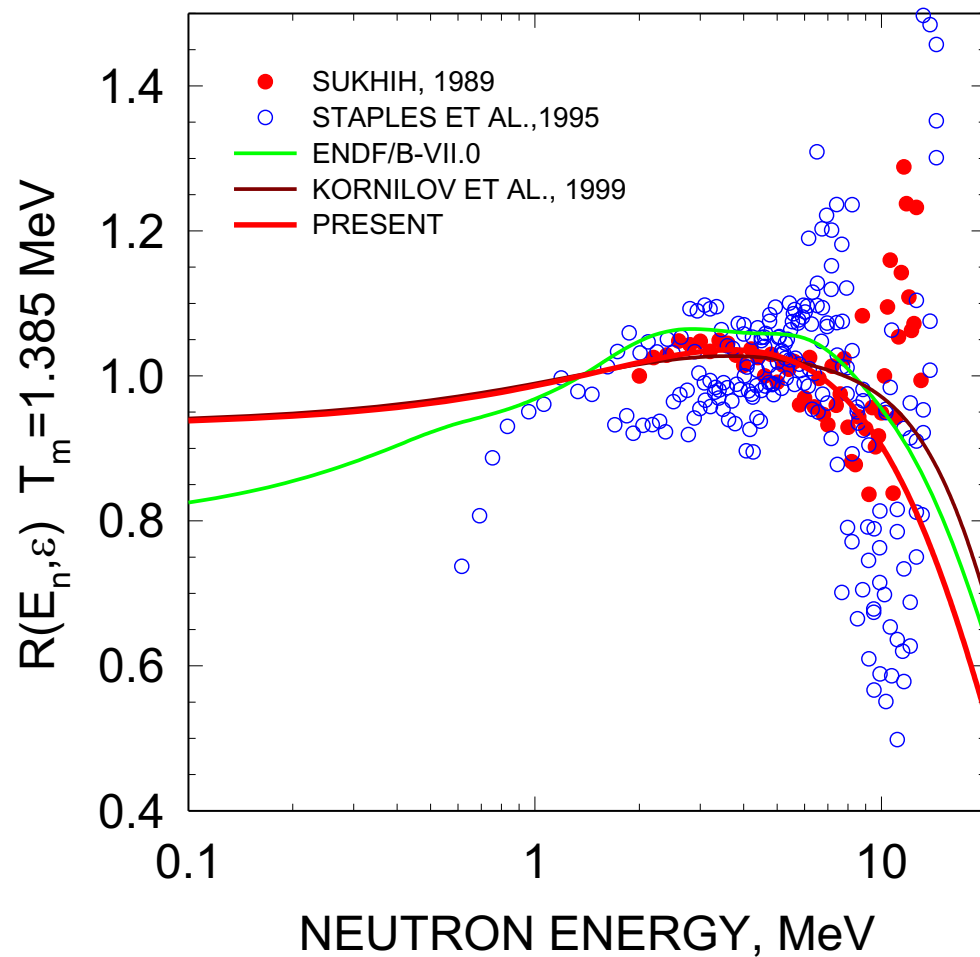


^{239}Pu FISSION NEUTRON SPECTRUM
 $E_n \sim 0.5 \text{ MeV}$

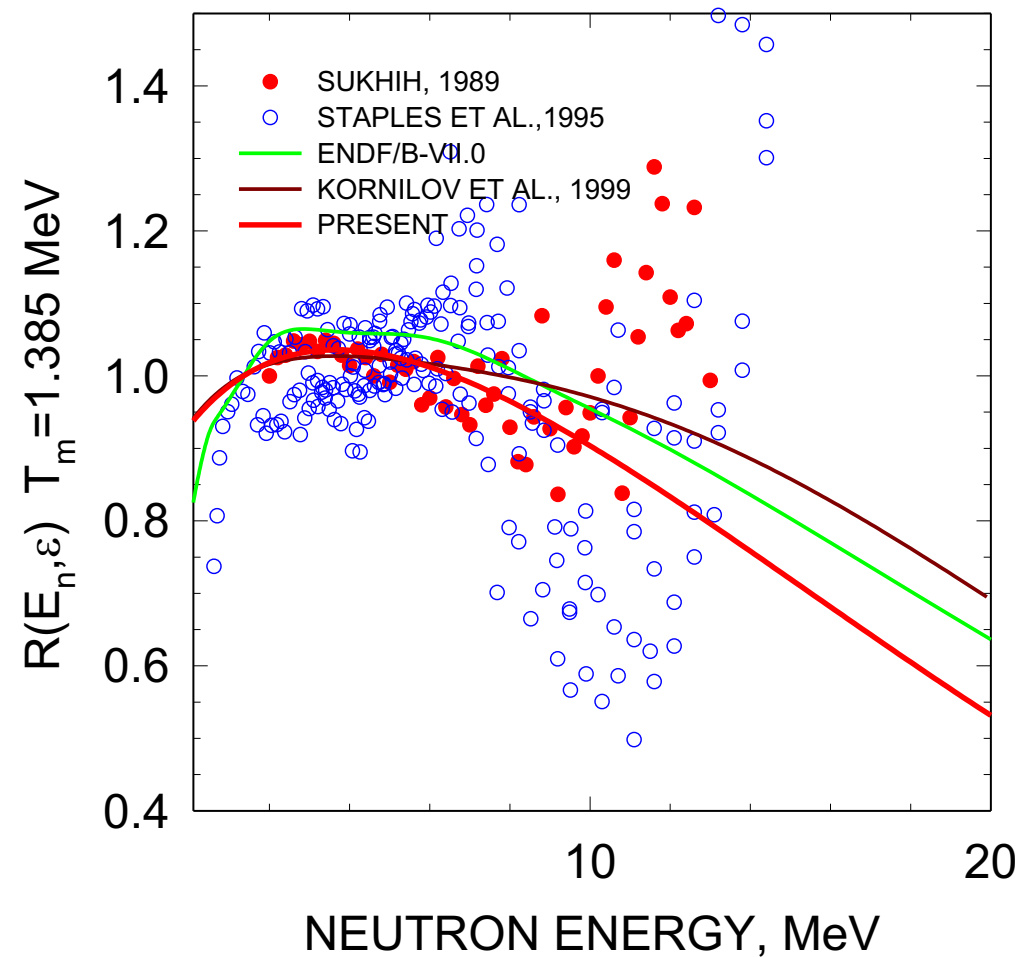


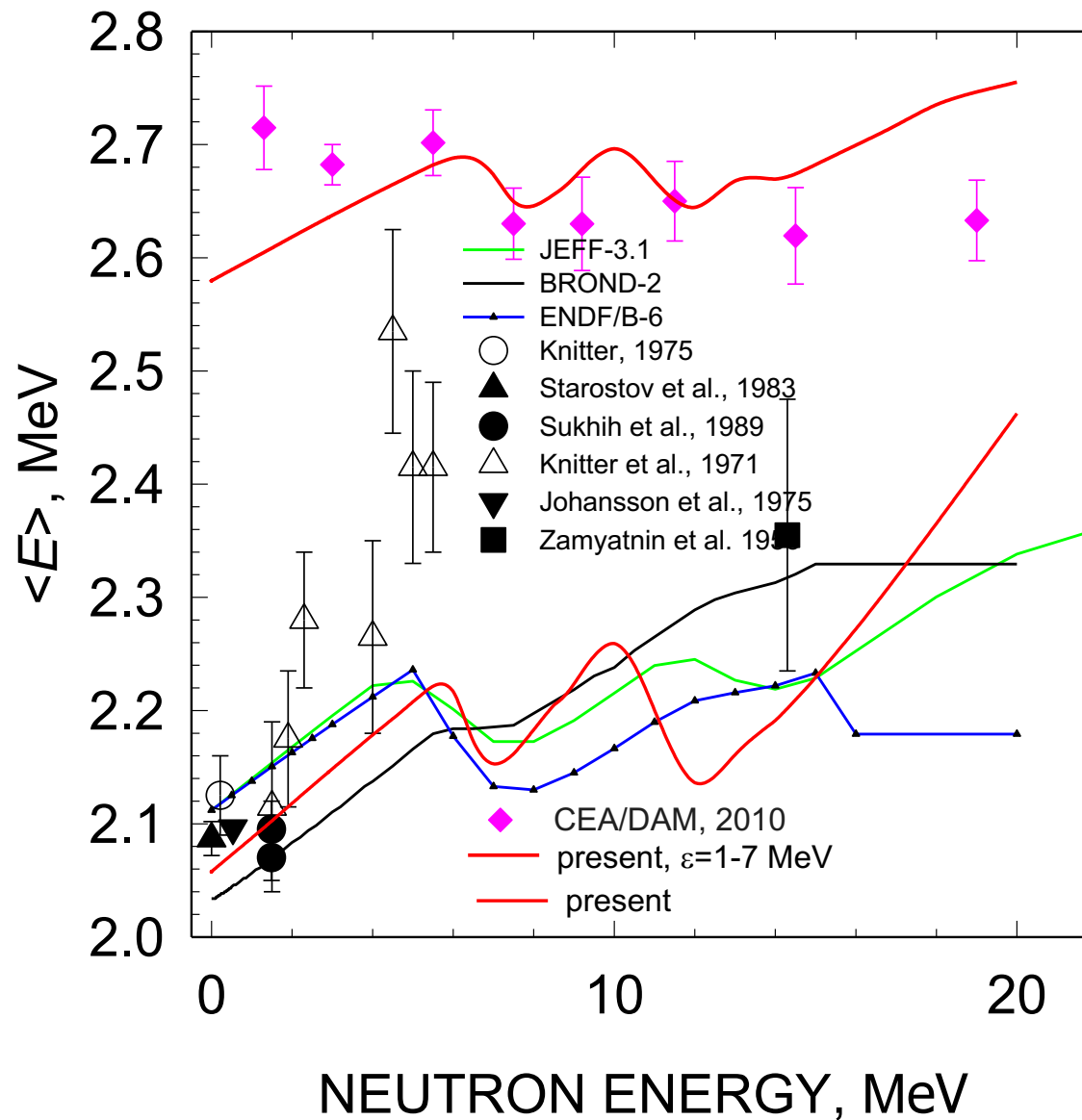


^{239}Pu FISSION NEUTRON SPECTRUM
 $E_n \sim 1.5 \text{ MeV}$



^{239}Pu FISSION NEUTRON SPECTRUM
 $E_n \sim 1.5 \text{ MeV}$





- Integral results are requested to enable the following system total results to be calculated: flux; production as a sum of fission production, (n,2n) production, and (n,3n) production; absorption as a sum of fission, capture, (n,2n), and (n,3n); and leakage from the outer edge of the system.
- The normalization of these results is not important, because a reactor can be critical at any power level. Specifically we consider the definition:

$$\rightarrow K_{eff} = \text{production} / \text{absorption} + \text{leakage}$$

- Nota Bene: since the **inhour**, **dollar**, and **cent** all depend upon the constituents and even structure of a reactor, reactivity is also measured in units defined as decimal fraction of unity. There are varying degree of usage and appropriation of the Canadian **mill-k**, equal to, the British **millinile**, the French “**pour cent mille**”, the Italian “**per centomila**”, the US percent **millirho**, all equal to and abbreviated **pcm**
- **LCT** Low Enriched Uranium-Compound-Thermal spectrum
- **PST** Plutonium-Solution-Thermal spectrum
- **HST** High Enriched Uranium-Solution-Thermal spectrum



Code				Tripoli-4.5		Tripoli-4.5		Tripoli-4.5		Δ (C-C)
Library				JEFF-3.1		JEFF-3.1.1		Maslov		
	Experiment			Calc.		Calc.	Δ	Calc.		
	K _{eff}	Unc.	K _{calc}	S.D.	K _{calc}	(C-C)	K _{calc}			
ICSBEP	Name			Fast Range						
IMF-007	Cyl. U Metal (10% 235U), thick 238U Reflector									
Big Ten	deta.	1.0045	70	0.99863	13	0.99878		0.99582		
	simp.	1.0045	70	0.99790	13	0.99770		0.99511		
Δ (C-E)				-623		-626	-2	-903	-278	
	t.z.h.	0.9948	130	0.98830	13	0.98838		0.98556		
Δ (C-E)				-650		-642	8	-924	-282	
IMF-012	Cyl. U Metal (16% 235U), Al and Steel, Reflected by Depleted-U									
ZPR(16%)	c-1	1.0007	270	1.00261	13	1.00262		1.00050		
Δ (C-E)				191		192	1	-20	-212	
IMF-10	Cyl U Metal (9% 235U), thick Depleted U Reflector									
ZPR-U9	c-1	0.9954	240	0.99181	13	0.99191		0.98880		
Δ (C-E)				-359		-349	10	-660	-311	
IMF-002	Nat. U Reflected Assembly of Enriched U Plates									
	c-1	1.0000	300	0.99216	10	0.99207		0.98997		
Δ (C-E)				-784		-793	-9	-1003	-210	
IMF-001	Bare Cyl. Conf. of Enriched and Natural U									
Jemima	c-2	1.0000	120	0.99837	12	0.99797		0.99725		
	c-3	1.0000	100	0.99741	12	0.99779		0.99622		
	c-4	1.0000	100	0.99850	12	0.99821		0.99691		
Average				0.99809		0.99799		0.99679		
Δ (C-E)				-191		-201	-10	-321	-120	
HMF-028	235U Sphere Reflected by Normal U using Flattop									
Flattop-25		1.0000	300	1.00210	11	1.00199		1.00150		
Δ (C-E)				210		199	-11	150	-49	
HMF-001	Bare, Highly Enriched U Sphere									
Godiva	c1	1.0000	100	0.99645	11	0.99668		0.99663		
	c2	1.0000	100	0.99660	11	0.99647		0.99645		
Average				0.99653		0.99658		0.99654		
Δ (C-E)				-347		-342	5	-346	-4	

up to ~ - 300 pcm
and Godiva, Flattop
intact

!! for JEFF-3.1.1

- ENDF/B-VII much
better there than !!
too much better??

Shaded grey means
C/E outside the exp.
Uncertainty (quoted)



Code				Tripoli-4.5		Tripoli-4.5		Tripoli-4.5		Δ (C-C)
Library				JEFF-3.1		JEFF-3.1.1		Maslov		
	Experiment			Calc.			Calc.	Δ	Calc.	
		K _{eff}	Unc.	K _{calc}	S.D.	K _{calc}	(C-C)	K _{calc}		
ICSBEP	Name			Thermal range U						
LCT-006	Low Enriched UO2 Fuel Rods with # Water-to-Fuel Volume Ratios									
	c-1	1.0000	200	0.99998	12	1.00071		1.00172	133	
	c-3	1.0000	200	1.00051	9	1.00127		1.00227		
	c-4	1.0000	200	0.99987	12	1.00082		1.00175		
	c-8	1.0000	200	1.00059	12	1.00118		1.00260		
	c-9	1.0000	200	1.00011	12	1.00067		1.00228		
	c-13	1.0000	200	0.99994	12	1.00042		1.00210		
	c-14	1.0000	200	0.99958	12	1.00036		1.00185		
	c-18	1.0000	200	0.99978	12	1.00049		1.00195		
Average				1.00005		1.00074		1.00206		
Δ (C-E)				5		74	69	206		
LCT-007	Water Reflected 4.738 Wt.% Enriched UO2 Fuel Rod Arrays									
Valduc	c-1	1.0000	160	0.99780	10	0.99844		1.00021	219	
	c-2	1.0000	160	0.99932	10	0.99975		1.00250		
	c-3	1.0000	160	0.99749	10	0.99821		1.00019		
	c-5	1.0000	160	0.99753	10	0.99806		1.00002		
	c-6	1.0000	160	0.99915	10	0.99988		1.00238		
	c-7	1.0000	160	0.99843	10	0.99915		1.00132		
Average				0.99829		0.99891		1.00110		
Δ (C-E)				-171		-109	62	110		
LCT-039	Incomplete Arrays of Water Reflected 4.738 Wt.% Enriched UO2 Fuel Rods									
Valduc	c-1	1.0000	140	0.99761	12	0.99799		1.00025		238
	c-4	1.0000	140	0.99665	12	0.99723		0.99969		
	c-6	1.0000	140	0.99767	12	0.99831		1.00073		
Average				0.99731		0.99784		1.00022		
Δ (C-E)				-269		-216	53	22		
Hector	k [∞] Experiments in Intermediate Neutron Spectra for 235U									
Hiss		1.0000	600	1.01003	13	1.00978		1.00986		
Δ (C-E)				1003		978	-26	986		
	Enriched Uranium Hydride sphere									
Topsy-NI		1.0000	400	1.00201	17	1.00182		1.00487	305	
Δ (C-E)				201		182	-19	487		
Topsy-UR		1.0000	400	1.00687	16	1.00733		1.00861		
Δ (C-E)				687		733	46	861	128	

up to ~ + 300
and Hiss intact
not Topsy

Better Valduc LCT-039
unique ...



Code				Tripoli-4.5		Tripoli-4.5		Tripoli-4.5	
Library				JEFF-3.1		JEFF-3.1.1		Maslov	
	Experiment			Calc.		Calc.	Δ	Calc.	Δ
		K _{eff}	Unc.	K _{calc}	S.D.	K _{calc}	Δ (C-C)	K _{calc}	(C-C)
ICSBEP	Name			Thermal range Pu					
PST-009	48" sphere, Al vessel, bare								
9.54 gPu/l	c-2A	1.0003	330	1.01893	11	1.01105		1.01272	
9.46 gPu/l	c-3A	1.0003	330	1.01927	11	1.01466		1.01634	
Average				1.01910		1.01285		1.01453	
Δ (C-E)				1880		1255	-625	1423	168
MCT-004	Mox 3.01 wt% PuO₂-UO₂ fuel rods,								
2.4 w/f ratio	c-1	1.0000	460	0.99683	13	0.99601		0.99882	
2.9 w/f ratio	c-4	1.0000	390	0.99707	13	0.99605		0.99922	
4.2 w/f ratio	c-7	1.0000	400	0.99779	13	0.99654		0.99938	
5.5 w/f ratio	c-10	1.0000	510	0.99783	13	0.99631		0.99870	
Average				0.99738		0.99622		0.99903	
Δ (C-E)				-262		-378	-116	-97	281
PST-001	11.5" sphere, water reflected								
73.0 gPu/l	c-1	1.0000	500	1.00186	12	1.00218		1.01057	
96.0 gPu/l	c-2	1.0000	500	1.00356	12	1.00403		1.01236	
119.0 gPu/l	c-3	1.0000	500	1.00665	12	1.00713		1.01539	
132.0 gPu/l	c-4	1.0000	500	1.00104	12	1.00144		1.00969	
140.0 gPu/l	c-5	1.0000	500	1.00505	12	1.00552		1.01354	
268.7 gPu/l	c-6	1.0000	500	1.00681	12	1.00732		1.01499	
Average				1.00416		1.00460		1.01275	
Δ (C-E)				416		460	44	1275	815
PST-011	16&18" sphere, bare								
34.9 gPu/l	16-1	1.0000	520	1.00669	13	1.00736		1.01498	
43.4 gPu/l	16-5	1.0000	520	1.00337	13	1.00370		1.01172	
Average				1.00503		1.00553		1.01335	
Δ (C-E)				503		553	50	1334	781
22.3 gPu/l	18-1	1.0000	520	0.99134	13	0.99160		0.99796	
27.5 gPu/l	18-6	1.0000	520	0.99708	13	0.99761		1.00428	
Average				0.99421		0.99460		1.00112	
Δ (C-E)				-579		-540	39	112	652

up to ~ + 800 pcm

More impact on its own
than the thermal xs
adjusted JEFF-3.1.1
- artificial neg. res.
-reduced nu prompt

Remark: which
benchmarks you choose
to fit ?? and why ??

Is this code, method,
continent dependent ??



Code				Tripoli-4.5		Tripoli-4.5		Tripoli-4.5	
Library				JEFF-3.1		JEFF-3.1.1		Maslov	
	Experiment			Calc.		Calc.	Δ	Calc.	Δ
		K _{eff}	Unc.	K _{calc}	S.D.	K _{calc}	Δ (C-C)	K _{calc}	(C-C)
PST-013	256-mm cyl, in air								
115 gPu/l	c-1	0.9980	400	1.00169	12	1.00203		1.00600	
115 gPu/l	c-2	0.9980	400	1.00157	12	1.00200		1.00623	
Average				1.00163		1.00202		1.00611	
Δ (C-E)				363		402	38	811	420
115 gPu/l	c-4	0.9965	520	0.99419	12	0.99460		0.99852	
Δ (C-E)				-231		-190	41	202	391
PMF-001	Bare Sphere of Pu-239 Metal								
Jezebel	c-1	1.0000	200	1.00025	15	0.99999		0.99889	
Δ (C-E)				25		-1	-26	-111	-110
PMF-002	Bare Sphere of Pu-239 Metal								
Jez. 240	c-1	1.0000	200	1.00430	15	1.00426		1.00332	
Δ (C-E)				430		426	-4	332	-94

Quite and
impact

Pu-239 PNFS impact on jezebel 240 !!, but every body think only Pu-240 in Jezebel 240 analysis.

Code				Tripoli-4.5		Tripoli-4.5		Tripoli-4.5	
Library				JEFF-3.1		JEFF-3.1.1		Maslov	
		Experiment		Calc.		Calc.	Δ	Calc.	Δ
		K _{eff}	Unc.	K _{calc}	S.D.	K _{calc}	Δ (C-C)	K _{calc}	(C-C)
ICSBEP	Name			Solutions					
HST001									
Mid	c-1	1.0004	600	0.99908	16	0.99917		1.00493	
Leakage	c-2	1.0021	720	0.99666	16	0.99695		1.00221	
Nitrate	c-3	1.0003	350	1.00237	16	1.00263		1.00809	
	c-4	1.0008	530	0.99929	16	0.99930		1.00448	
	c-5	1.0001	490	0.99974	16	1.00024		1.00470	
	c-6	1.0002	460	1.00314	16	1.00375		1.00802	
	c-7	1.0008	400	0.99882	16	0.99909		1.00456	
	c-8	0.9998	380	0.99890	16	0.99929		1.00471	
	c-9	1.0008	540	0.99483	16	0.99477		1.00069	
Average		1.0006		0.99920		0.99947		1.00471	
Δ (C-E)				-139		-112	26	412	524
HST009									
High	c-1	0.9990	430	1.00064	16	1.00143		1.00623	
Leakage	c-2	1.0000	390	1.00144	16	1.00163		1.00694	
Fluoride	c-3	1.0000	360	1.00099	16	1.00134		1.00669	
	c-4	0.9986	350	0.99559	16	0.99573		1.00099	
Average		0.9994		0.99966		1.00003		1.00521	
Δ (C-E)				26		63	37	581	518
HST010									
Fluoride	c-1	1.0000	290	1.00104	16	1.00108		1.00615	
	c-2	1.0000	290	1.00122	16	1.00156		1.00616	
	c-3	1.0000	290	0.99872	16	0.99896		1.00360	
	c-4	0.9992	290	0.99666	16	0.99700		1.00203	
Average		0.9998		0.99941		0.99965		1.00448	
Δ (C-E)				-39		-15	24	468	483

up to ~ + 500 pcm
a first !!

For those
ENDF/B-VII ~ JEFF-
3.1 ~ JENDL-3.3

Are solution more
sensitive to spectral
data ??

Really reliable ??

Fluor, Nitrogen data
impact ?



HST010								
Fluoride	c-1	1.0000	290	1.00104	16	1.00108		1.00615
	c-2	1.0000	290	1.00122	16	1.00156		1.00616
	c-3	1.0000	290	0.99872	16	0.99896		1.00360
	c-4	0.9992	290	0.99666	16	0.99700		1.00203
Average		0.9998		0.99941		0.99965		1.00448
Δ (C-E)				-39		-15	24	468
HST011								
Fluoride	c-1	1.0000	230	1.00473	16	1.00519		1.00922
	c-2	1.0000	230	1.00062	16	1.00142		1.00544
Average				1.00267		1.00331		1.00733
Δ (C-E)				267		331	63	733
HST012								
	c-1	0.9999	580	1.00115	15	1.00126		1.00346
Δ (C-E)				125		136		356
HST013								
ORNL-1	c-1	1.0012	260	0.99880	16	0.99816		1.00117
ORNL-2	c-2	1.0007	360	0.99791	16	0.99962		1.00008
ORNL-3	c-3	1.0003	360	0.99416	16	0.99452		0.99654
ORNL-4	c-4	1.0003	360	0.99591	16	0.99641		0.99811
Average		1.0006		0.99669		0.99718		0.99897
Δ (C-E)				-393		-345	48	-165
HST018								
Nitrate	c-1	1.0000	340	0.98956	16	0.98980		0.99483
	c-2	1.0000	460	0.98503	16	0.98535		0.99030
	c-3	1.0000	420	0.98832	16	0.98877		0.99369
Average				0.98764		0.98797		0.99294
Δ (C-E)				-1236		-1203	34	-706
HST019								
	c-1	1.0000	410	0.99691	16	0.99708		1.00204
Δ (C-E)				-309		-292	17	204
HST032								
ORNL-10		1.0015	260	0.99881	16	0.99921		1.00036
Δ (C-E)				-269		-229	41	-114

483

220

179

497

495

114

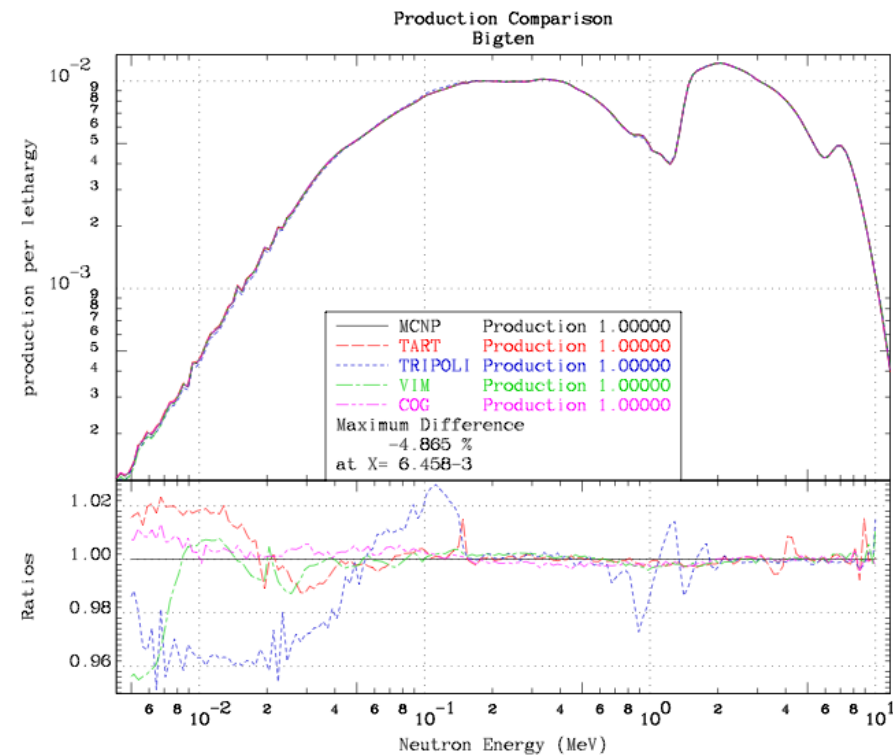
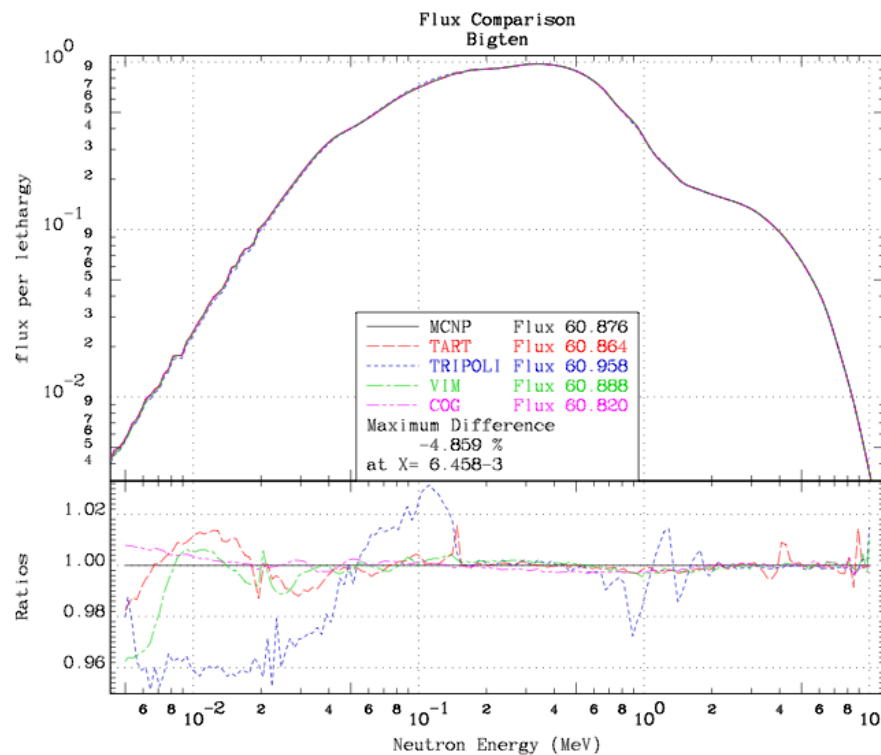
up to ~ + 500 pcm
a first !!

More attention need
to be pay to solution
benchmarks

495 pcm swing

- Contrary to common (reactor physicist) belief PFNS were
 - poorly described, evaluated and certainly used (only one thermal spectra to create a matrix)
 - in essence questionable
- PFNS can impact benchmarks K_{eff} as potently as cross section, i.e.
 - ☞ + 500 pcm for solutions (unique amongst all libraries)
 - ☞ - 300 pcm for thermal U but + 300 pcm for fast U
 - ☞ + 800 pcm for thermal Pu but -300 for fast Pu
- Emitted spectra are as important as cross section or even angular distribution but not for fission

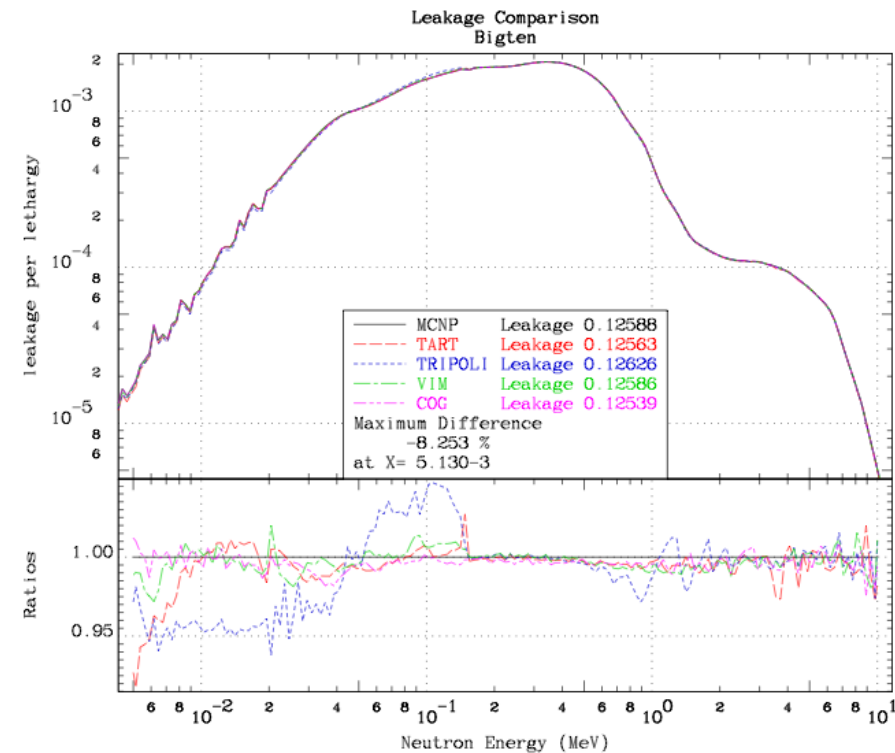
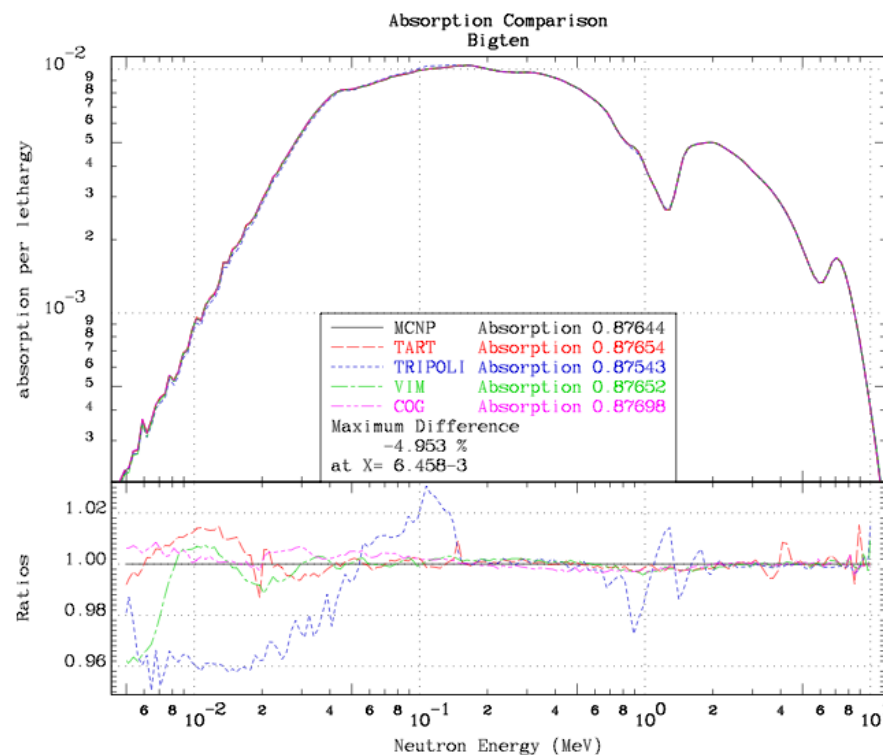
- Neutron fluxes and production, 660 groups



Absorption Leakage K-eff

MCNP	.884520	.121459	0.99406
TART	.884691	.121389	0.99402
TRIPOLI	.884657	.121288	0.99409

- Absorption and leakage, 660 groups



Absorption Leakage K-eff

MCNP	.884520	.121459	0.99406
TART	.884691	.121389	0.99402
TRIPOLI	.884657	.121288	0.99409



- The biases induced by the actual pretty much identical (ENDF/B, JEFF or JENDL) U's and Pu's PNFS are
 - rarely accounted for and certainly not negligible
 - parts of the compensating effects
 - now understandable, having been probed by Monte Carlo codes analysis
- New, more physical and better described prompt fission spectra have been, are being produced and need to be accounted for, particularly when cross section fitting or adjustment are foreseen or have been already imbedded in a given library (nu, inelastic level,...)



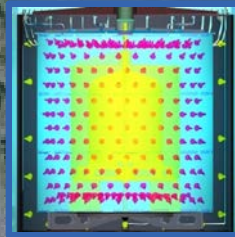
- Mostly form deterministic simulation results
- Monte Carlo and Deterministic results do not always agree on fast ICSBEP benchmark and good Monte Carlo on thermal are rare
- Monte Carlo results on big power full core are rare
- Big power core differs feedbacks from little leaky ones, but both are interpreted in the same way
- Simulation methods data forms interpretation issues exists
- Indubitably, all nuclear data contains compensating data, but the past 20 years revealed, interpretation issues
 - U^{238} capture, U^{238} inelastic
 - O^{16} capture above 2.4 MeV !! For UOx and not H_2O
 - U^{235} pnfs and their interpretation
 - H_2O thermal below 10 eV

Reminding all that reactors are made of real materials, molecules (UOx , H_2O , etc..) and not pure isotope

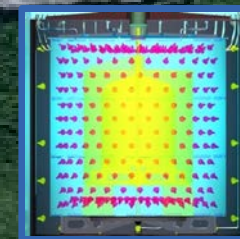
- For pure reactor physics applications, and by that I mean reactor operational simulations, it is now clear that “they” have all the nominal data needed, 444 power reactors running but ^{239}Pu C/E 10% & ^{235}U number density 5%
- In the light of reactor physics latest software and analysis tools development what clearly missing are
 - The use of nuclear data forms variance-covariance information:
 - Energy wise
 - Channel wise, Isotope wise
 - Matrix wise; nu, sigma, spectra
 - The true, realistic software/methods biases
 - The correlation between the macro-quantities, data forms used by the simulation tools
- Solely new fuels, claddings, operational (energy) regimes may change, modify those requirements

Double Chooz

**Two N4-REP
reactors
(2*4.27GW_{th})**



**Near detector @400m
Overburden 120mwe
Running since 2014**



**Far detector @1050m
Overburden 300 mwe
Running since 2011**

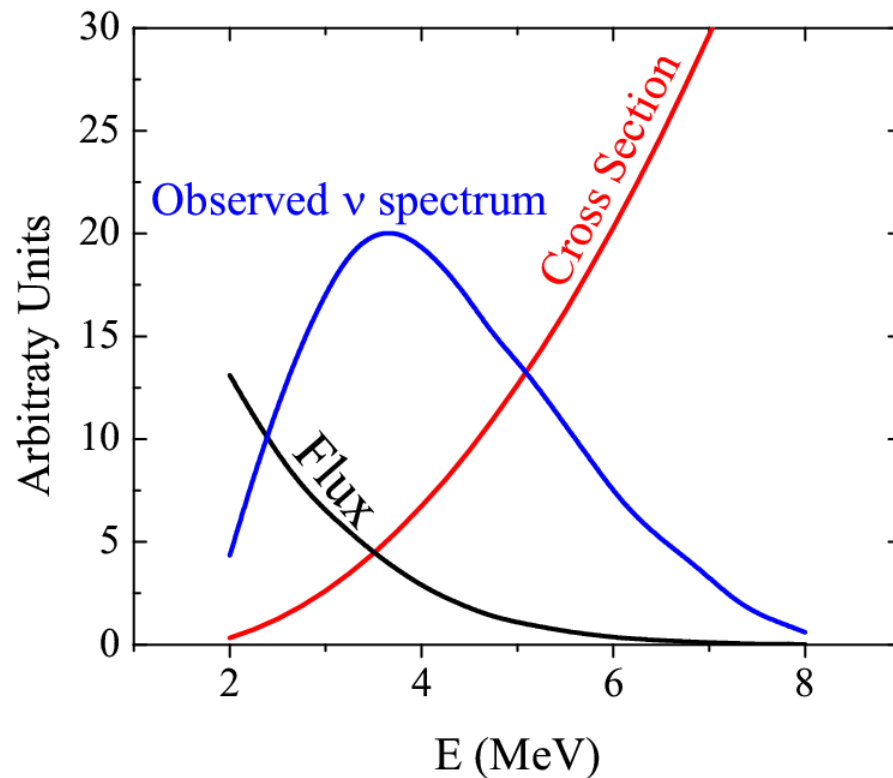
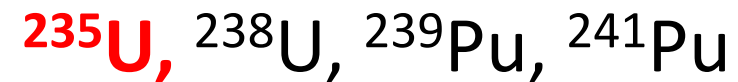
- In a nuclear reactor there are about 6 β -decays, and hence neutrinos, per fission or about 2×10^{20} neutrinos per second per GW of thermal power.
- Fortunately, there are only four isotopes whose fission make up more than 99% of all reactor neutrinos with an energy above the inverse β -decay threshold: ^{235}U , ^{239}Pu , ^{241}Pu and ^{238}U
- Nonetheless, the resulting neutrino flux is a superposition of thousands of β -decay branches of the fission fragments of those four isotopes and thus, a first principle calculation is challenging, even with modern nuclear structure data
 - Inverted measured@ILL total β -spectra for thermal fission of ^{235}U , ^{239}Pu and ^{241}Pu (no fast ^{238}U)
 - Summation method

The reactor $\bar{\nu}_e$ anomaly

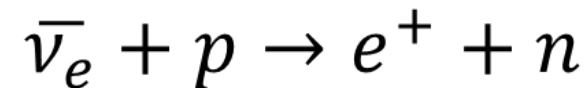
$$\text{Flux} \sim 5 \cdot 10^{20} \bar{\nu}_e / s$$

$$\langle N_\nu \rangle \sim 6$$

Principal originators of contributors



Detection through inverse β decay on proton



Reaction threshold : ~ 1.8 MeV

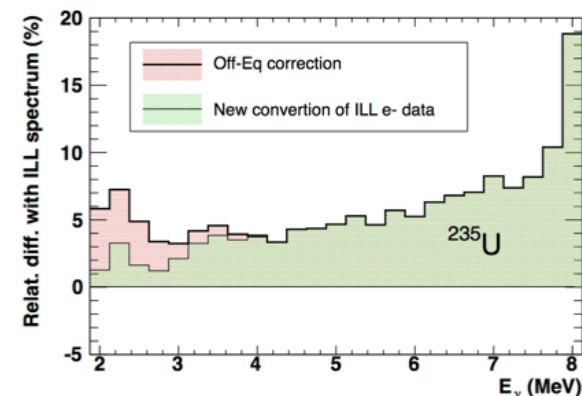
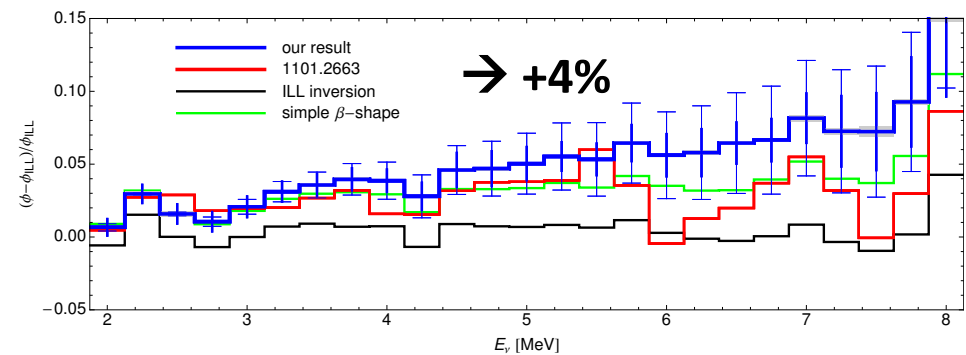
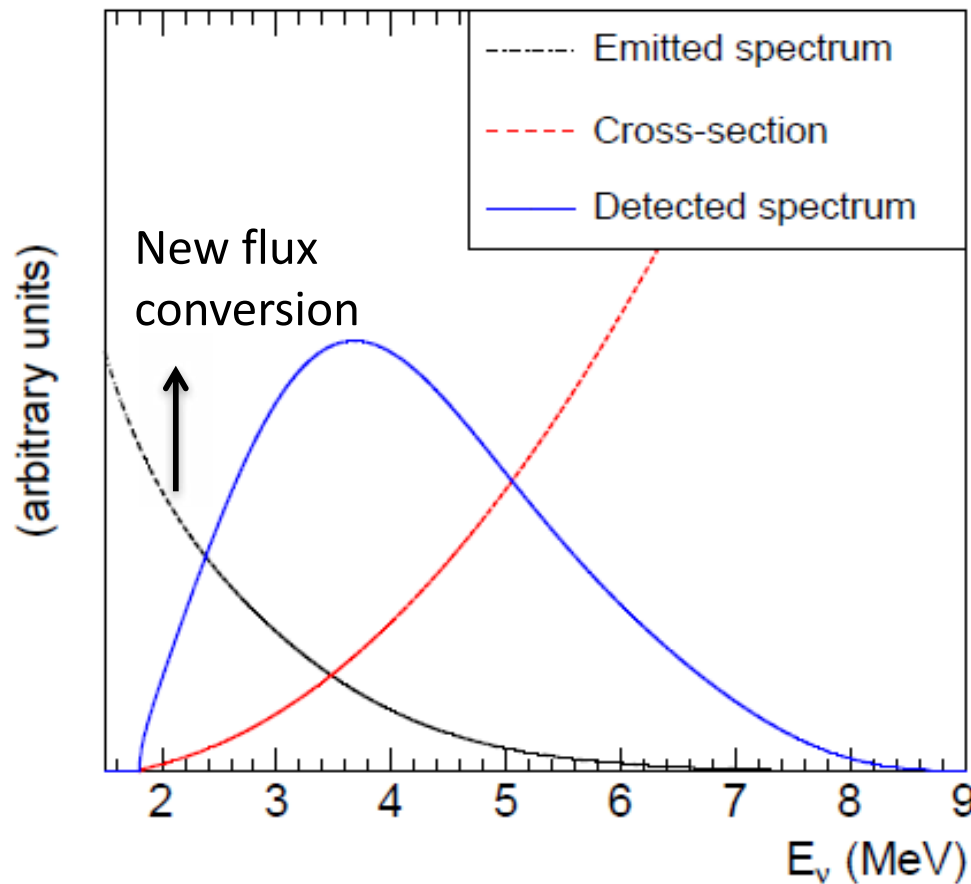
$$\langle \sigma \rangle \sim 10^{-43} \text{ cm}^2$$

The reactor ν_e anomaly, appeared in 2011

New conversion of ILL beta spectra

Th. Mueller et al, Phys. Rev. C83,054615 (2011)

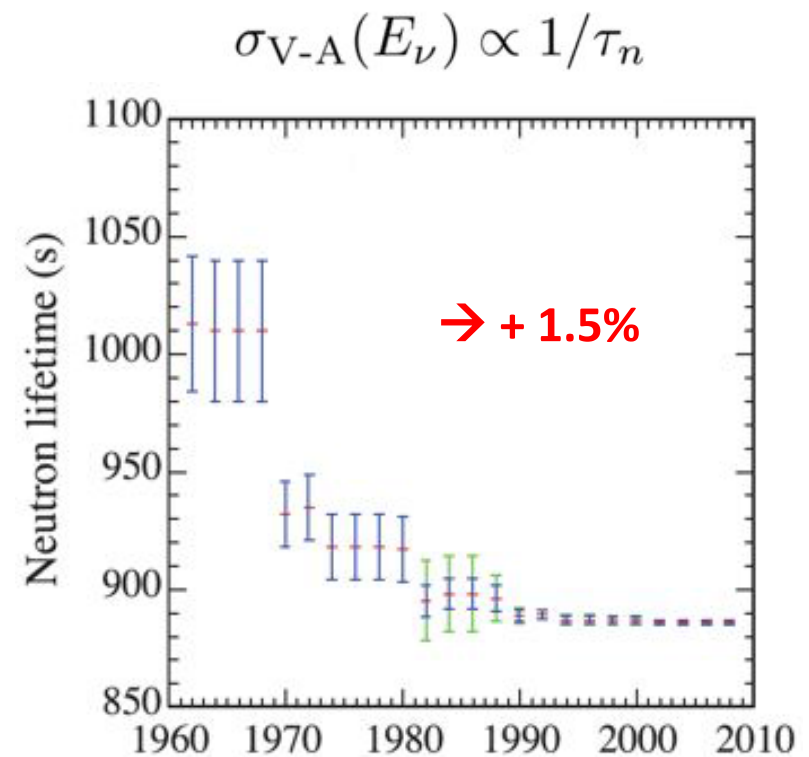
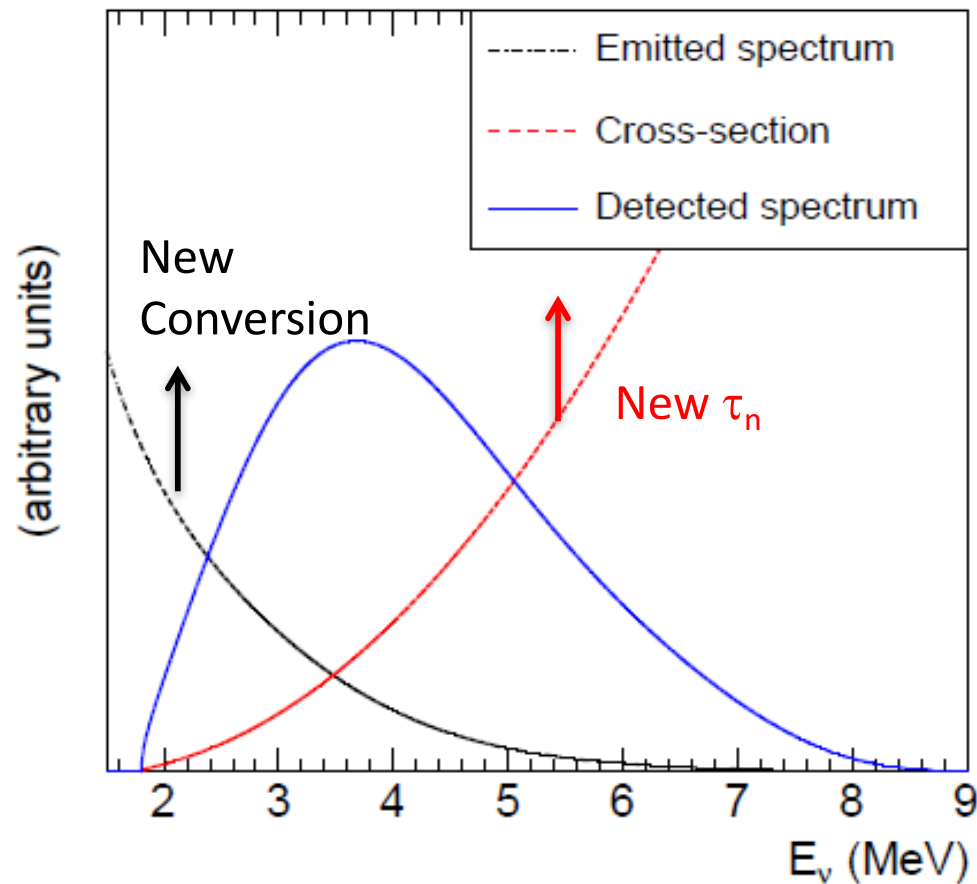
P. Huber, Phys. Rev. C84, 024617(2011)



Accumulation
of long lived
isotopes

→ +1%

Re-evaluation of $\sigma_{\text{interaction}}$

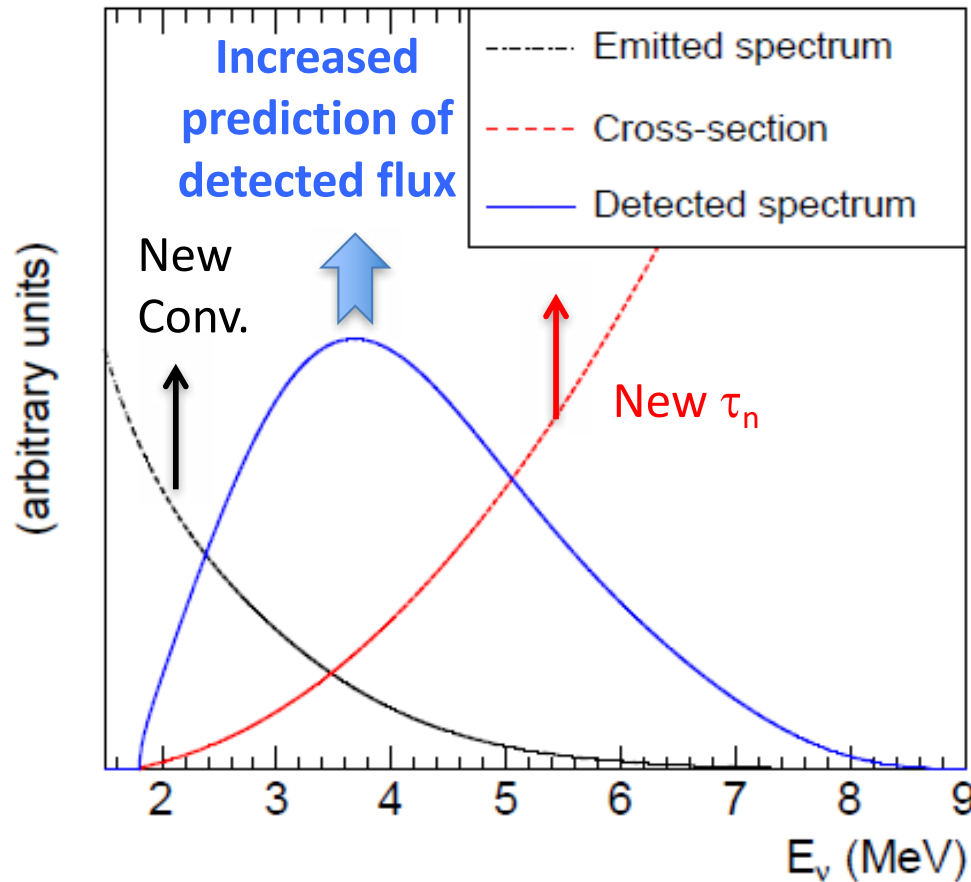


PRD 83, 073006 (2011)

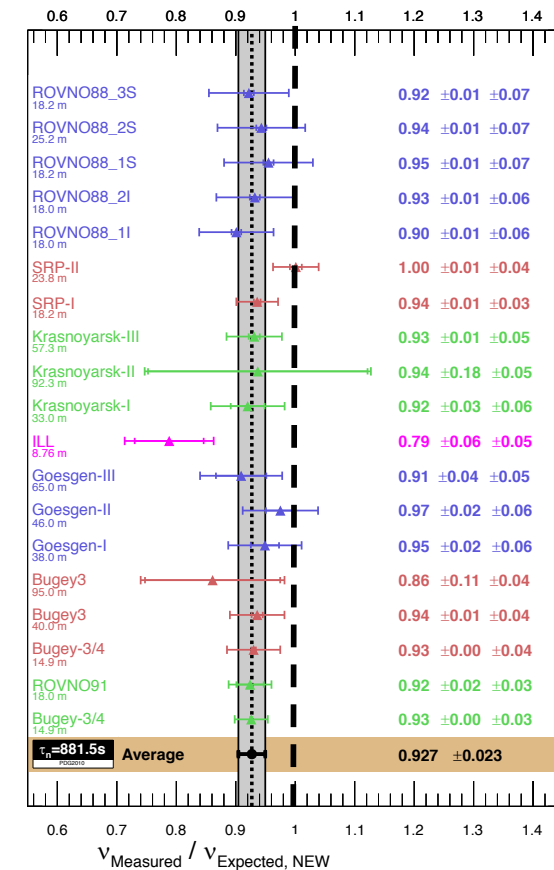


Reanalysis of reactor short baselines experiments

G. Mention et al., Phys. Rev. D83, 073006 (2011)

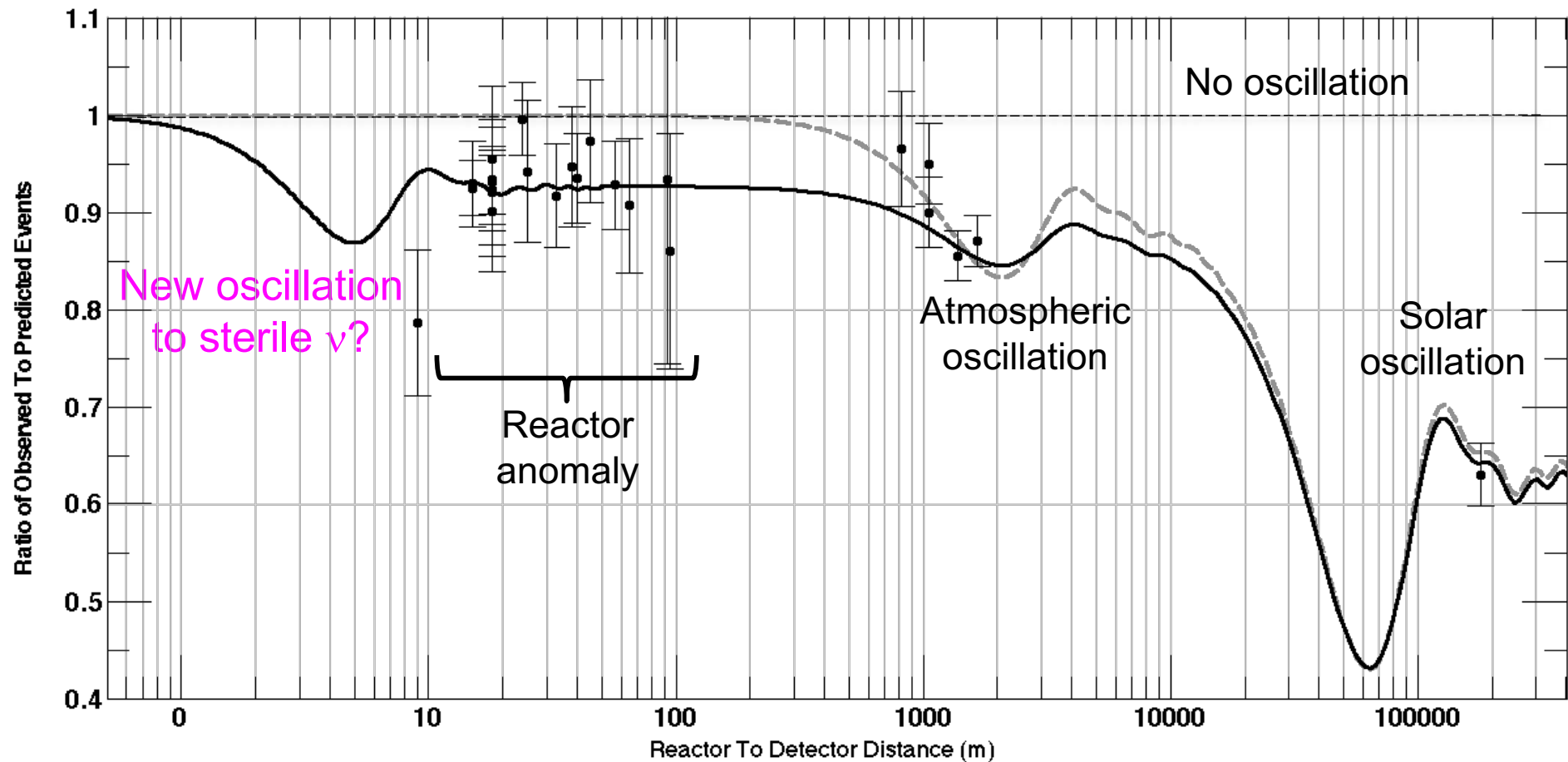


Significant increase of the prediction by 6.5%





Survey of 19 short baseline (<100 m) reactor antineutrino experiments Observed/predicted averaged event ratio: $R=0.935 \pm 0.024$



**Deficit of ~6.5%, or 3 times the calculated uncertainty
In the spectrum**

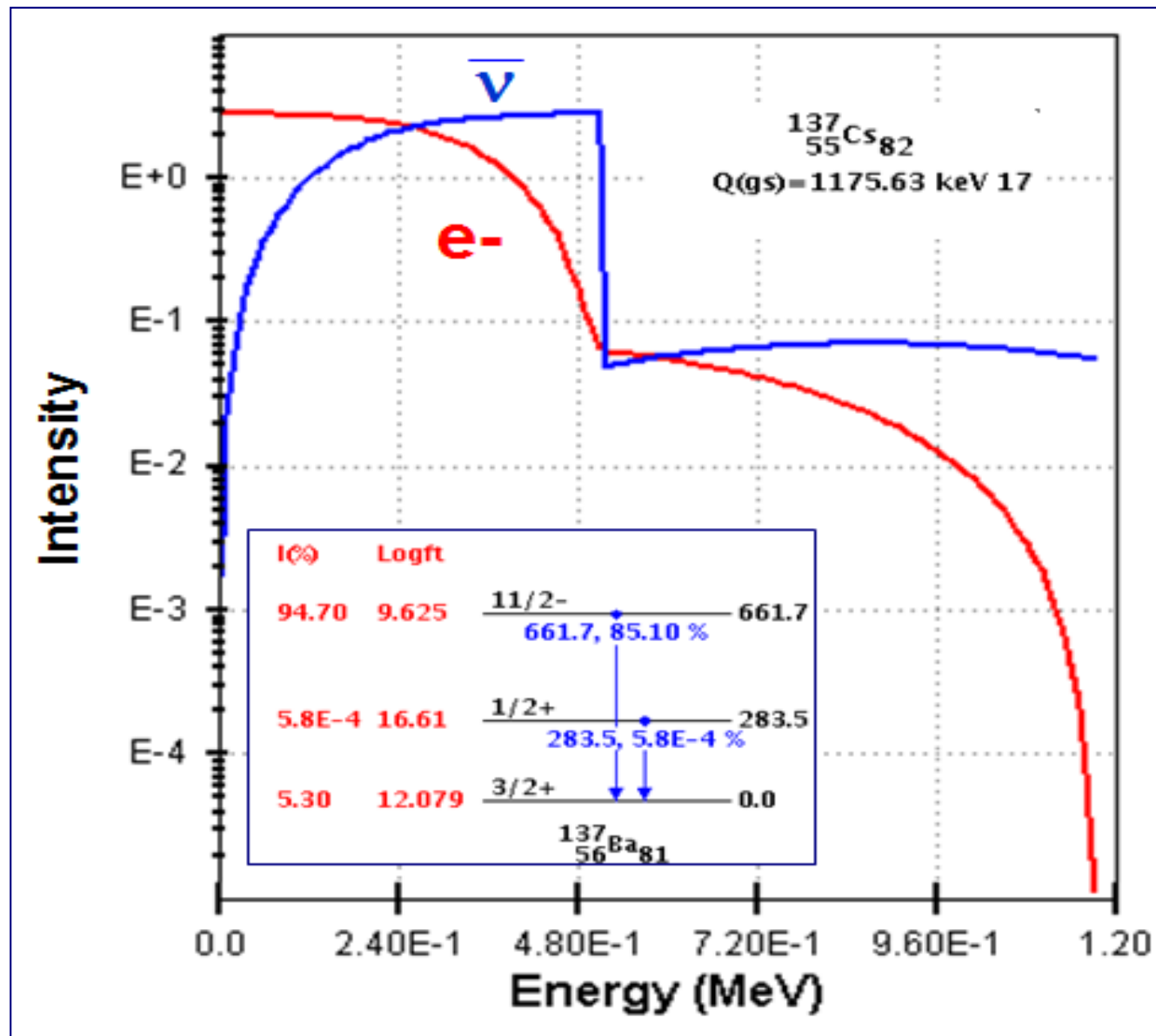


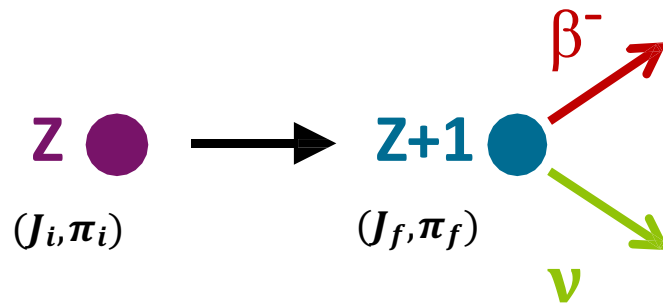
IAEA

60 Years

Atoms for Peace and Development

^{137}Cs β^- & $\bar{\nu}_e$ spectra





ΔJ	$\pi_i \pi_f$	Classification
0, 1	1	Allowed
0, 1	-1	1 st fnu
> 1	$(-1)^{ \Delta J }$	$ \Delta J $ th fnu
> 1	$(-1)^{ \Delta J -1}$	$(\Delta J - 1)$ th fu

$$\Delta J = |J_f - J_i|$$

fnu : forbidden non-unique
 fu : forbidden unique

Basics of beta decay, the **most common assumption**

- **Systematic comparison** with 130 **experimental shape factors**

Recent precise measurements of **⁶³Ni** and **²⁴¹Pu** beta spectra

- **Improvements** of the calculation to include **atomic effects**



Similarly we obtain for the space components

$$\langle p | \mathbf{V} + \mathbf{A} | n \rangle = i u_p^\dagger \gamma_4 \gamma_5 (1 + \lambda \gamma_5) u_n = \sqrt{\frac{(W_n + M_n)}{2W_n}} \sqrt{\frac{(W_p + M_p)}{2W_p}} \begin{pmatrix} 0 & i\sigma \\ i\sigma & 0 \end{pmatrix} \lambda \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix} \times \left\{ \left(\frac{\sigma \mathbf{p}}{W_p + M_p} \chi_p^{m'} \right)^+ \sigma \chi_n^m + \left(\chi_p^{m'} \right)^+ \sigma \frac{\sigma \mathbf{p}}{W_n + M_n} \chi_n^m - \lambda \left(\chi_p^{m'} \right)^+ \sigma \chi_n^m - \lambda \left[\left(\frac{\sigma \mathbf{p}}{W_p + M_p} \chi_p^{m'} \right)^+ \sigma \frac{\sigma \mathbf{p}}{W_n + M_n} \chi_n^m \right] \right\}. \quad (6.38)$$

This equals to

$$\langle p | \mathbf{V} + \mathbf{A} | n \rangle = \sqrt{\frac{(W_n + M_n)}{2W_n}} \sqrt{\frac{(W_p + M_p)}{2W_p}} \left\{ \left(\chi_p^{m'} \right)^+ \frac{\sigma \mathbf{p}_p}{W_p + M_p} \sigma \chi_n^m + \frac{\mathbf{p}_p - i(\sigma \times \mathbf{p}_p)}{W_n + M_n} \chi_n^m - \lambda \left(\chi_p^{m'} \right)^+ \sigma \chi_n^m - \lambda \left[\left(\chi_p^{m'} \right)^+ \frac{\sigma \mathbf{p}_p}{W_p + M_p} \sigma \frac{\sigma \mathbf{p}_n}{W_n + M_n} \chi_n^m \right] - \frac{(\mathbf{p}_p \mathbf{p}_n) \sigma + (\sigma \mathbf{p}_p \mathbf{p}_n + \mathbf{p}_p (\sigma \mathbf{p}_n) - i(\mathbf{p}_p \times \mathbf{p}_n))}{(W_p + M_p)(W_n + M_n)} \right\}. \quad (6.39)$$

Finally we obtain for the space components

$$\langle p | \mathbf{V}(0) + \mathbf{A}(0) | n \rangle = \sqrt{\frac{(W_n + M_n)}{2W_n}} \sqrt{\frac{(W_p + M_p)}{2W_p}} \times \left\{ \left[\frac{\mathbf{p}_p}{W_p + M_p} + \frac{\mathbf{p}_n}{W_n + M_n} \right] (\chi_p^{m'})^+ \chi_n^m + (\chi_p^{m'})^+ \times \left[\frac{i(\sigma \times \mathbf{p}_p)}{W_p + M_p} - \frac{i(\sigma \times \mathbf{p}_n)}{W_n + M_n} \right] \chi_p^m - \lambda (\chi_p^{m'})^+ \sigma \chi_n^m + \lambda \frac{\mathbf{p}_p \mathbf{p}_n}{(W_p + M_p)(W_n + M_n)} \{ (\chi_p^{m'})^+ \sigma \chi_n^m \} + \lambda \frac{i(\mathbf{p}_p \times \mathbf{p}_n)}{(W_p + M_p)(W_n + M_n)} \times (\chi_p^{m'})^+ \chi_n^m - \lambda \left[(\chi_p^{m'})^+ \frac{(\sigma \mathbf{p}_p) \mathbf{p}_n + \mathbf{p}_p (\sigma \mathbf{p}_n)}{(W_p + M_p)(W_n + M_n)} \chi_n^m \right] \right\}. \quad (6.40)$$

$$-\frac{i}{2M_A} F_M(q^2)(\mathbf{P} \times \mathbf{q}) \sigma - F_S(q^2) q_0 + \frac{1}{4(2M_A)^2} F_S(q^2) q_0 (\mathbf{P}^2 - \mathbf{q}^2) - \frac{i}{2(2M_A)^2} F_S(q^2) q_0 (\mathbf{P} \times \mathbf{q}) \sigma \} \chi^M, \quad (9.15)$$

$$\langle \phi_f(p_f) | A_0(0) | \phi_i(p_i) \rangle = N(\chi^{M_i})^+ \left\{ -\frac{1}{2M_A} F_A(q^2)(\mathbf{P} \sigma) - \frac{q_0}{2M_A} F_P(q^2)(\mathbf{q} \sigma) - F_T(q^2)(\mathbf{q} \sigma) + \frac{1}{4(2M_A)^2} F_T(q^2) \times [(\mathbf{P} \mathbf{q})(\sigma \mathbf{P} + \sigma \mathbf{q}) - (\sigma \mathbf{q})(\mathbf{P}^2 - \mathbf{q}^2)] \right\} \chi^M, \quad (9.16)$$

$$\langle \phi_f(p_f) | \mathbf{V}(0) | \phi_i(p_i) \rangle = N(\chi^{M_i})^+ \left\{ \frac{1}{2M_A} F_V(q^2) \mathbf{P} + \frac{i}{2M_A} F_V(q^2)(\sigma \times \mathbf{q}) + i F_M(q^2)(\sigma \times \mathbf{q}) - \frac{1}{2M_A} F_M(q^2) q_0 \mathbf{q} - \frac{i}{4M_A} F_M(q^2) q_0 (\sigma \times \mathbf{P}) - F_S(q^2) \mathbf{q} + \frac{1}{4(2M_A)^2} F_S(q^2) \mathbf{q} (\mathbf{P}^2 - \mathbf{q}^2) - \frac{i}{2(2M_A)^2} F_S(q^2) \mathbf{q} \times [(\mathbf{P} \times \mathbf{q}) \sigma] - \frac{i}{2(2M_A)^2} F_M(q^2) \mathbf{P} ((\mathbf{P} \times \mathbf{q}) \sigma) - \frac{i}{4(2M_A)^2} \times F_M(q^2)(\mathbf{P}^2 + \mathbf{q}^2)(\sigma \times \mathbf{q}) + \frac{i}{2(2M_A)^2} F_M(q^2)(\mathbf{P} \mathbf{q})(\sigma \times \mathbf{P}) \right\} \chi^M, \quad (9.17)$$

$$\langle \phi_f(p_f) | \mathbf{A}(0) | \phi_i(p_i) \rangle = N(\chi^{M_i})^+ \left\{ -F_A(q^2) \sigma + \frac{1}{2(2M_A)^2} \times F_A(q^2) \mathbf{P}^2 \sigma - \frac{1}{4(2M_A)^2} F_A(q^2)(\mathbf{P}^2 + \mathbf{q}^2) \sigma - \frac{i}{2(2M_A)^2} \times F_A(q^2)(\mathbf{P} \times \mathbf{q}) - \frac{1}{2(2M_A)^2} F_A(q^2)[(\sigma \mathbf{P}) \mathbf{P} - (\sigma \mathbf{q}) \mathbf{q}] + \frac{1}{2M_A} F_T(q^2)[(\mathbf{P} \mathbf{p}) \sigma - (\mathbf{q} \mathbf{p}) \sigma] - F_T(q^2) q_0 \sigma + \frac{1}{2(2M_A)^2} F_T(q^2) q_0 \mathbf{P}^2 \sigma - \frac{1}{4(2M_A)^2} F_T(q^2) q_0 (\mathbf{P}^2 + \mathbf{q}^2) \sigma - \frac{i}{2(2M_A)^2} F_T(q^2) q_0 (\mathbf{P} \times \mathbf{q}) - \frac{1}{2(2M_A)^2} F_T(q^2) q_0 [(\sigma \mathbf{P}) \mathbf{P} - (\sigma \mathbf{q}) \mathbf{q}] - \frac{1}{2M_A} F_P(q^2)(\sigma \mathbf{q}) \mathbf{q} \right\} \chi^M, \quad (9.18)$$

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SPECIAL FORMULAE

$$+ \sqrt{\frac{2}{3}} \left(\int \frac{r I'(r)}{R} \beta \gamma_5 T_{121} \right) \} \mp \frac{f_P}{R} (W_0 R \pm \frac{2}{3} \alpha Z) {}^D \mathcal{M}_{110}^{(0)}(1, 1, 1, 1) \quad (14.101)$$

$${}^A F_{121}^{(0)} = \pm \lambda {}^A \mathcal{M}_{121}^{(0)} - \frac{f_T}{R} \left[\frac{5}{\sqrt{3}} {}^C \mathcal{M}_{111}^{(0)} - (W_0 R \pm \frac{2}{3} \alpha Z) {}^A \mathcal{M}_{121}^{(0)} \right] \mp \frac{f_P}{R} 5 \sqrt{\frac{2}{3}} {}^D \mathcal{M}_{110}^{(0)} \quad (14.102)$$

$${}^A F_{121}^{(0)}(1, 1, 1, 1) = \pm \lambda {}^A \mathcal{M}_{121}^{(0)}(1, 1, 1, 1) - \frac{f_T}{R} \left\{ \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) [5 I(r) + r I'(r)] \beta T_{111} \right\} - (W_0 R \pm \frac{2}{3} \alpha Z) {}^A \mathcal{M}_{121}^{(0)}(1, 1, 1, 1) \} \mp \frac{f_P}{R} \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) [5 I(r) + r I'(r)] \beta \gamma_5 T_{110} \} \quad (14.103)$$

$${}^V F_{211}^{(0)} = - {}^V \mathcal{M}_{211}^{(0)} - \frac{f_M}{R} (W_0 R \pm \frac{2}{3} \alpha Z) {}^C \mathcal{M}_{211}^{(0)} \quad (14.104)$$

$${}^V F_{220}^{(0)} = {}^V \mathcal{M}_{220}^{(0)} + \frac{f_M}{R} \sqrt{(10)} {}^C \mathcal{M}_{211}^{(0)} \pm \frac{f_S}{R} (W_0 R \pm \frac{2}{3} \alpha Z) {}^V \mathcal{M}_{220}^{(0)} \quad (14.105)$$

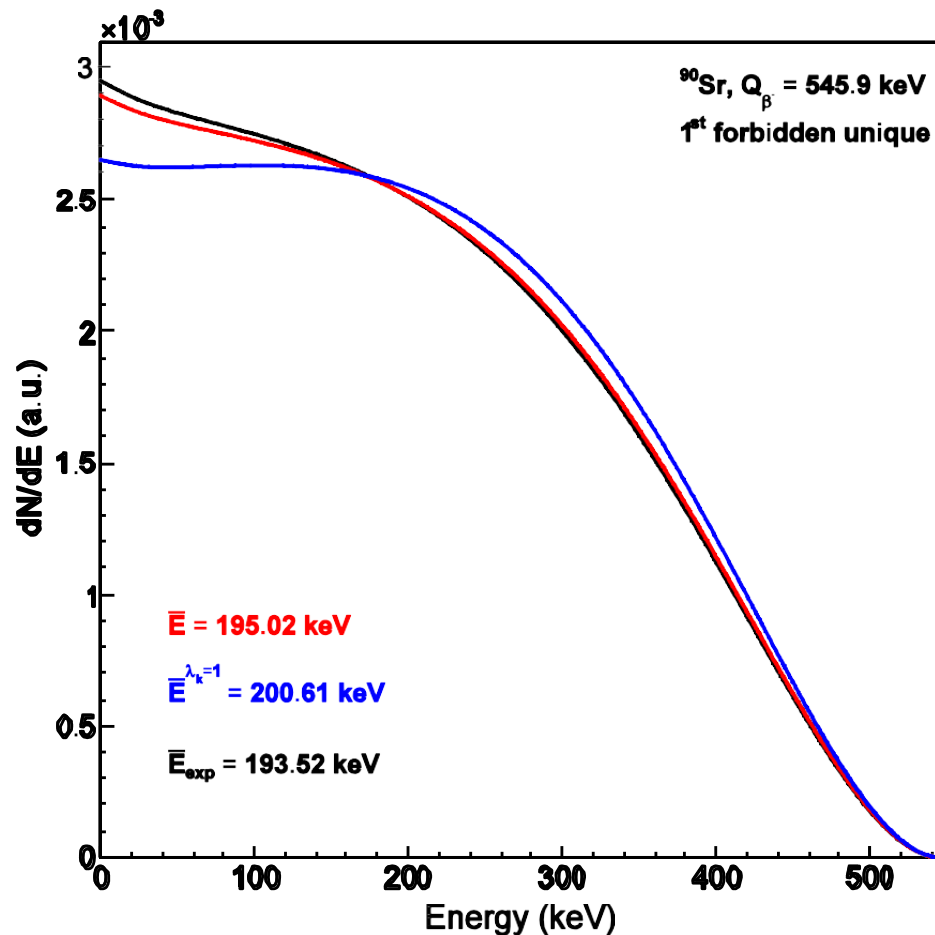
$${}^V F_{220}^{(0)}(1, 1, 1, 1) = {}^V \mathcal{M}_{220}^{(0)}(1, 1, 1, 1) + \frac{f_M}{R} \left\{ \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) [5 I(r) + r I'(r)] \beta T_{211} \right\} + \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) r I'(r) \beta T_{231} \} \pm \frac{f_S}{R} (W_0 R \pm \frac{2}{3} \alpha Z) {}^V \mathcal{M}_{220}^{(0)}(1, 1, 1, 1) \quad (14.106)$$

$${}^A F_{221}^{(0)} = \pm \lambda {}^A \mathcal{M}_{221}^{(0)} + \frac{f_T}{R} \left[\sqrt{(15)} {}^C \mathcal{M}_{211}^{(0)} - (W_0 R \pm \frac{2}{3} \alpha Z) {}^A \mathcal{M}_{221}^{(0)} \right] \quad (14.107)$$

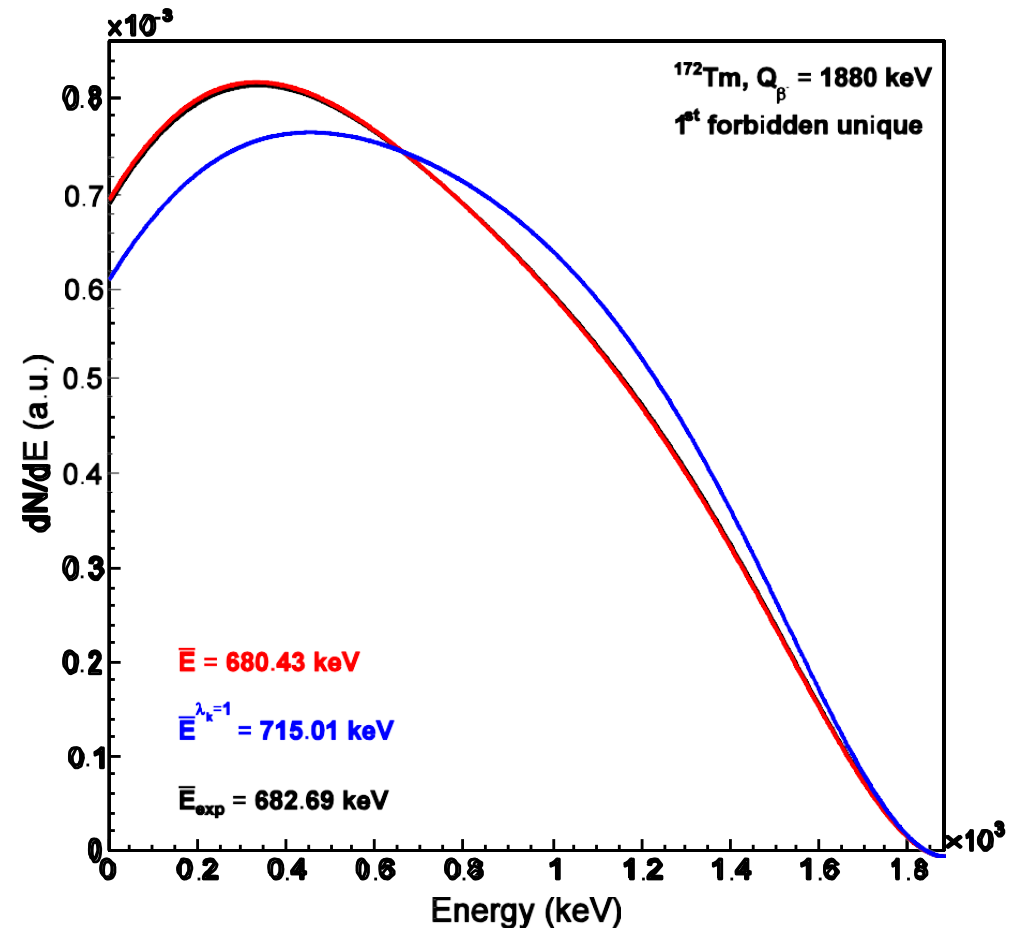
$${}^A F_{221}^{(0)}(1, 1, 1, 1) = \pm \lambda {}^A \mathcal{M}_{221}^{(0)}(1, 1, 1, 1) + \frac{f_T}{R} \left\{ \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) [5 I(r) + r I'(r)] \beta T_{211} \right\} - \sqrt{\frac{2}{3}} \left(\int \frac{r}{R} \right) r I'(r) \beta T_{231} \} - (W_0 R \pm \frac{2}{3} \alpha Z) {}^A \mathcal{M}_{221}^{(0)}(1, 1, 1, 1) \} \quad (14.108)$$

H. Behrens, W. Bühring, *Electron Radial Wave functions and Nuclear Beta Decay*, Oxford Science Publications (1982)

More than 600 pages !!



Mean energy disagrees by **3.6 %**
High influence at low energy



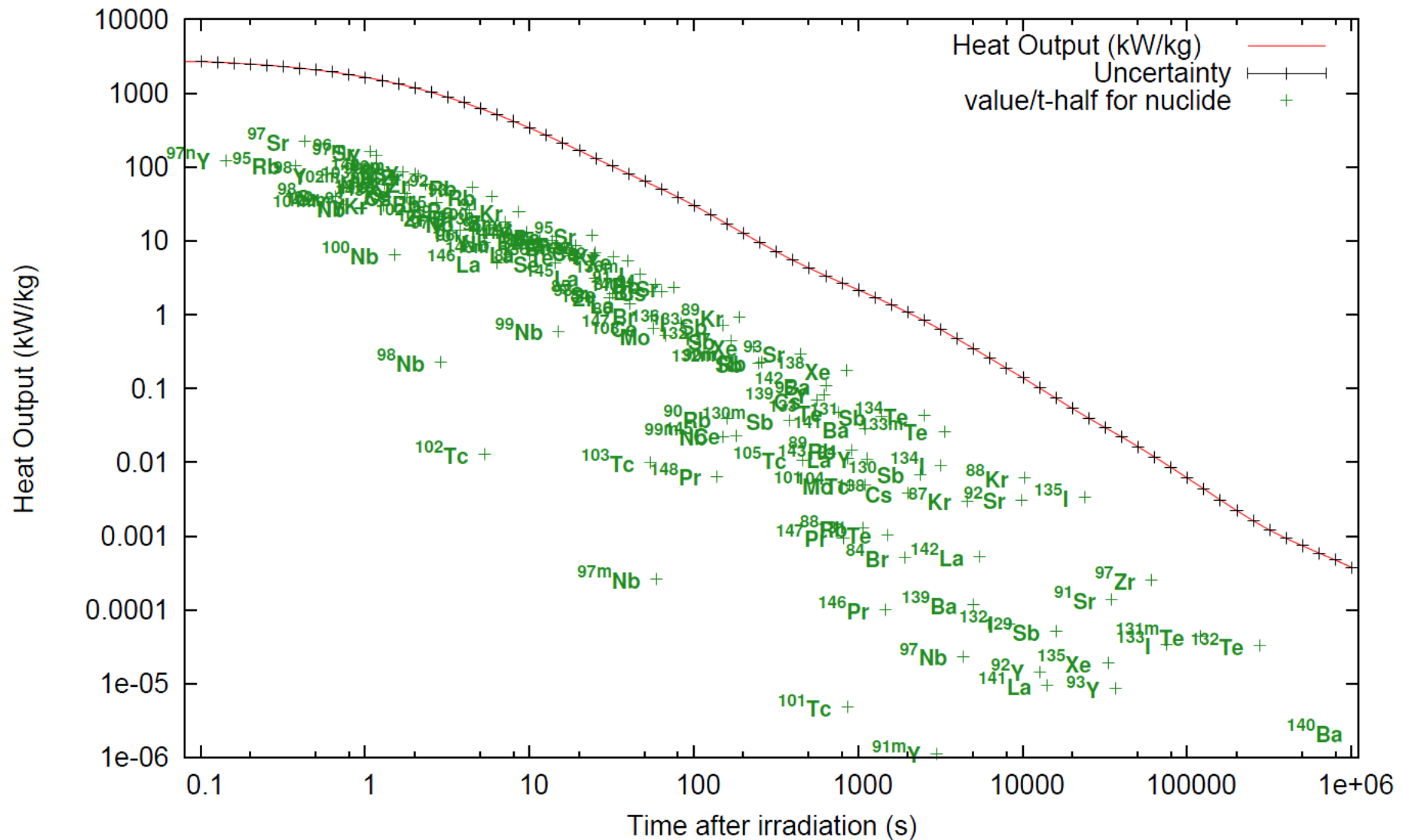
Mean energy disagrees by **4.6 %**
High influence at low energy and on the overall shape of the spectrum

$\lambda_k = 1$ approximation, usually **bad approximation !!**

ξ **approximation** is correct **only** for $\sim 50 \%$ of the **1st forbidden non-unique**

Thermal ^{235}U pulse generates a large inventory...

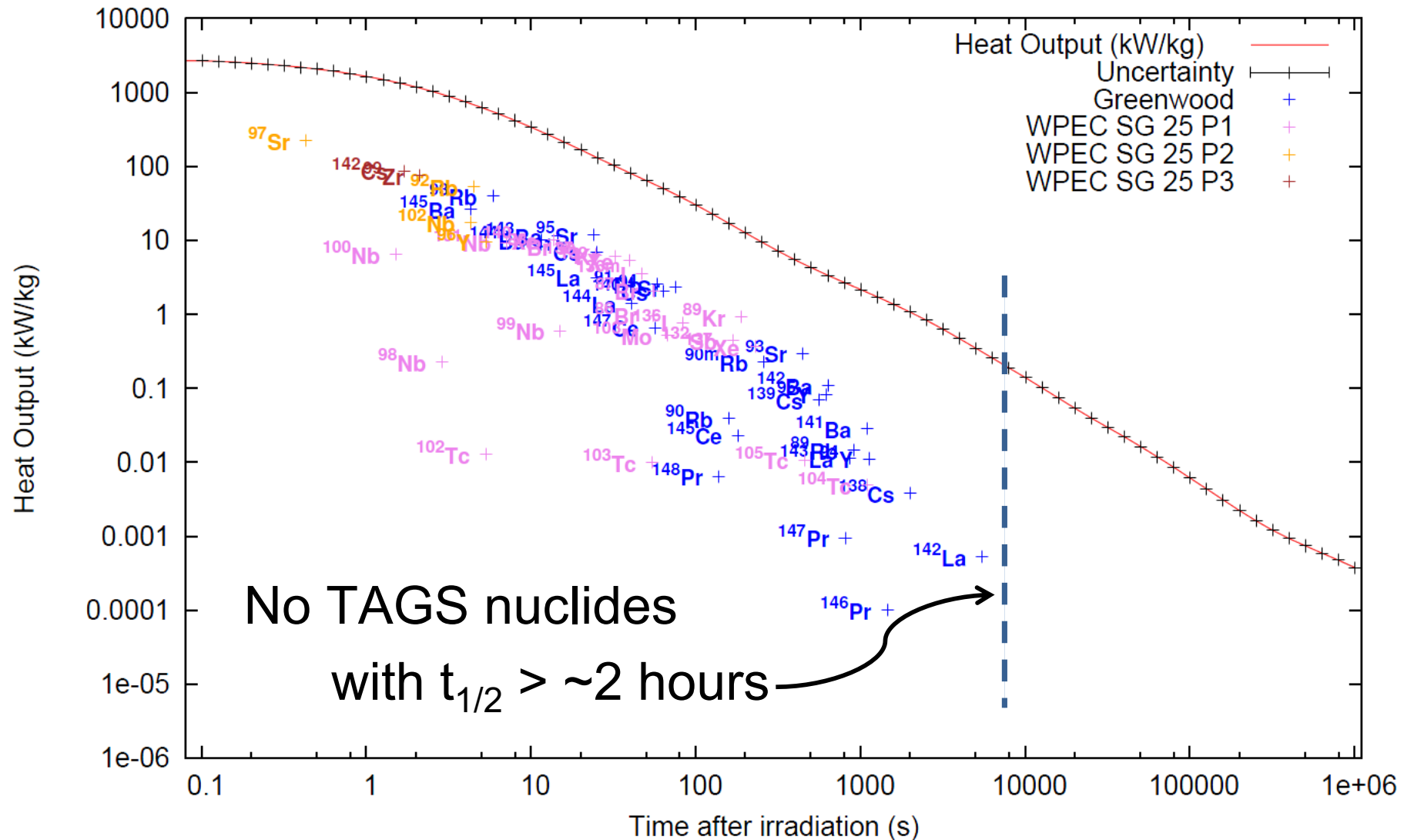
Each nuclide at $(x,y)=(t_{1/2},\text{heat}(t_{1/2}))$



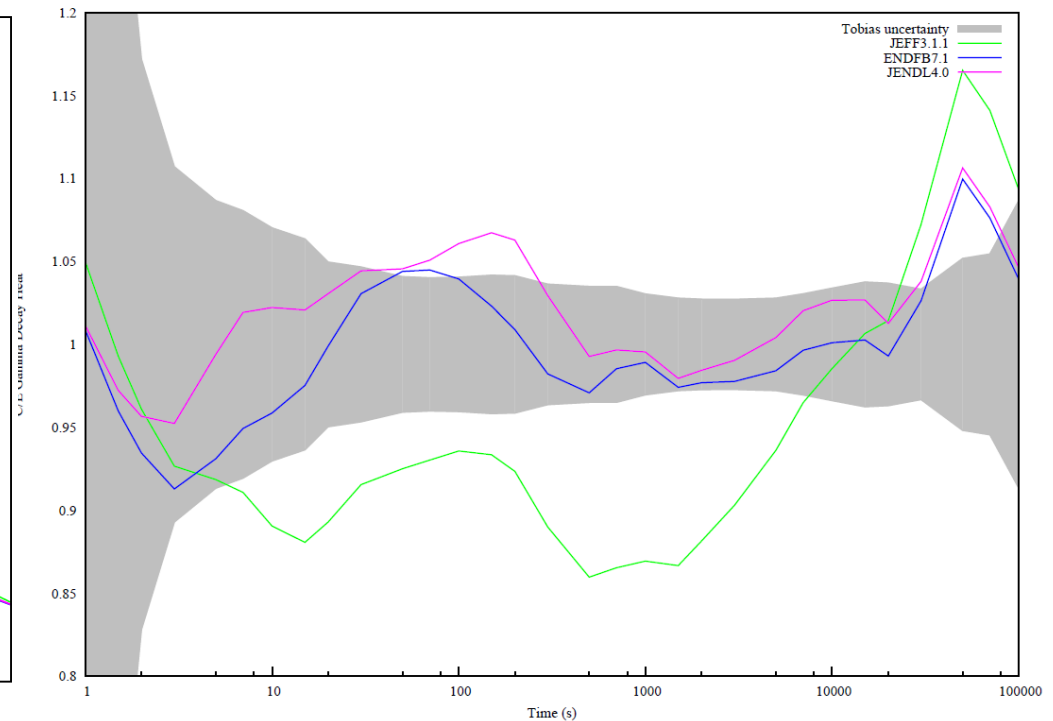
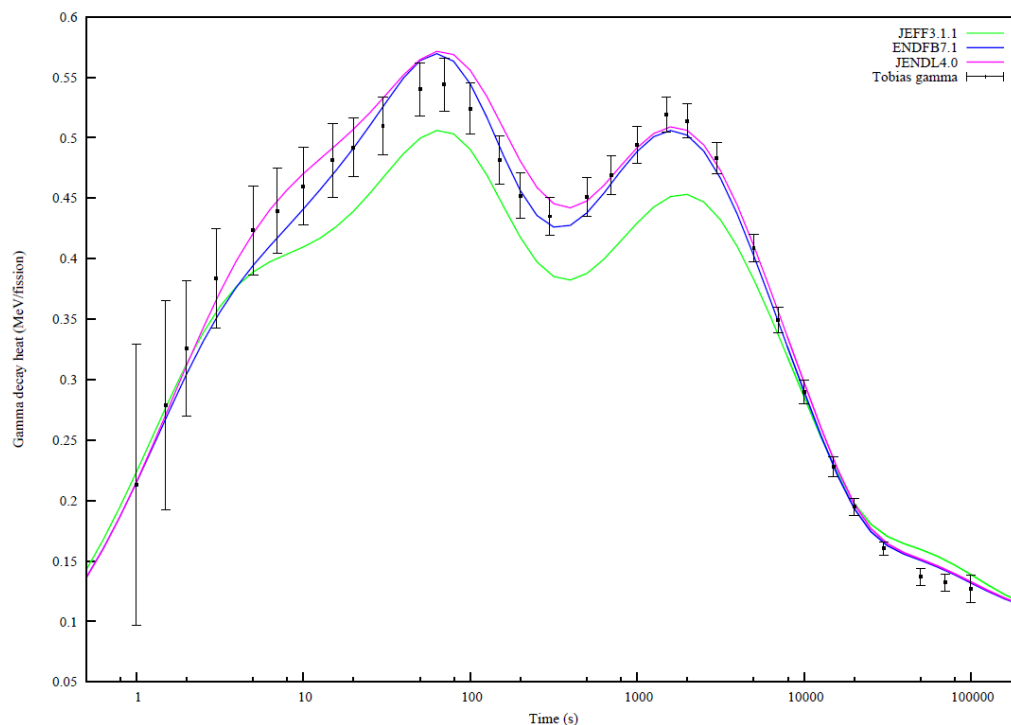


Fission products

Blue = Greenwood nuclides and WPEC SG 25 P1, P2, P3 are priority 1, 2, 3 nuclides with requested TAGS by subgroup 25



- Underestimation of high-energy gamma feeding due to poor detector efficiency: Pandemonium effect
- Better simulation with TAGS results, recently added in JENDL 4.0 and ENDF/B-VII.1, not JEFF-3.1.1 decay files !!



Compensation → too high beta for “fixed” total



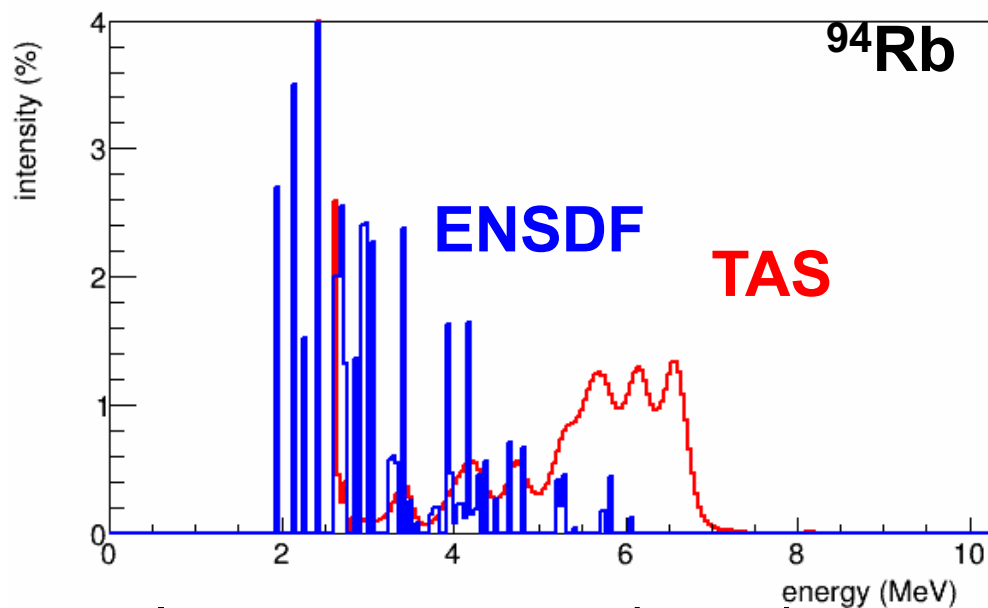
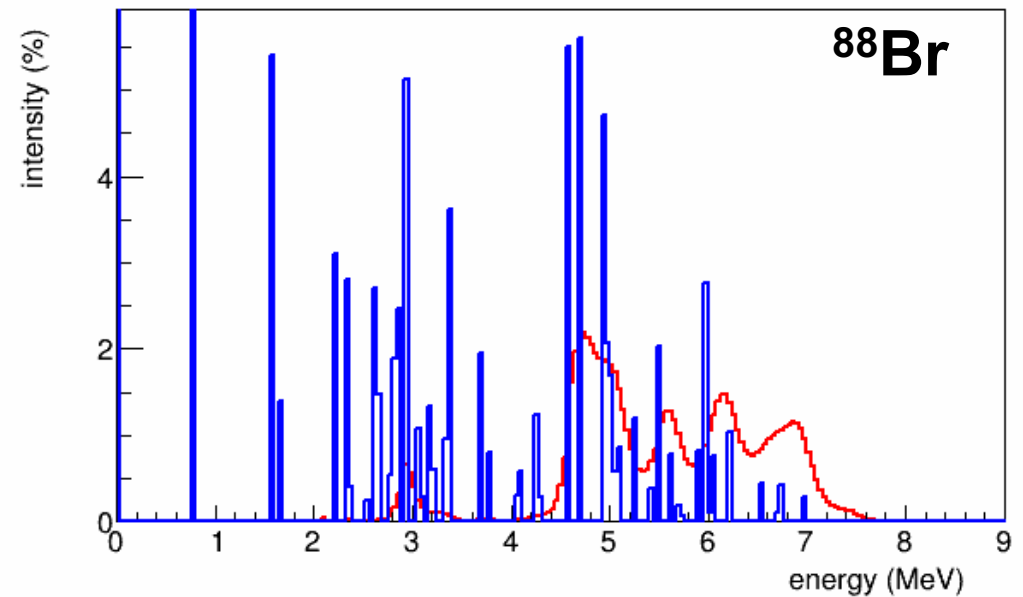
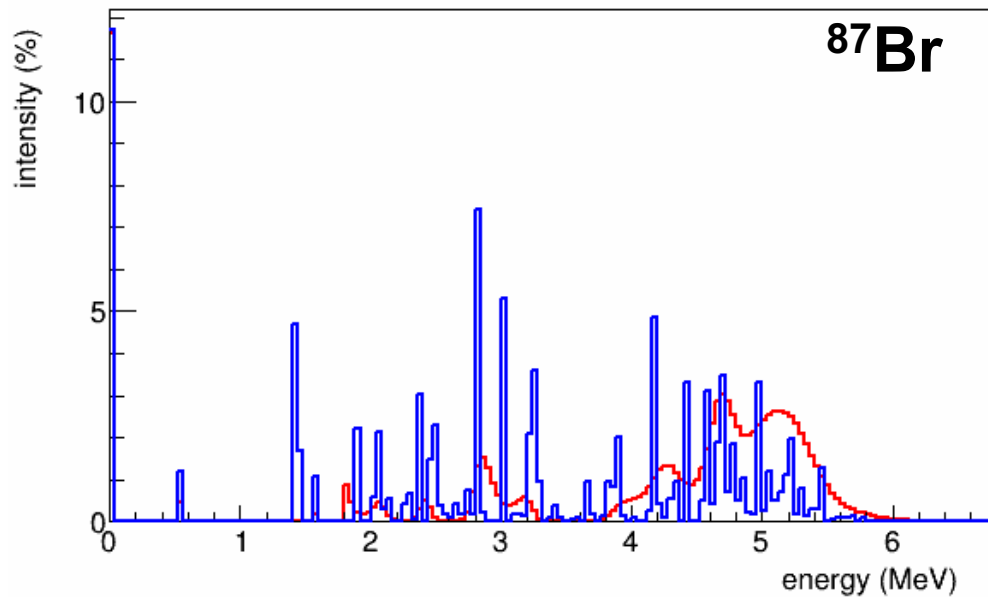
- Below are the dominant nuclides and their **gamma** heat contribution at 800s after pulse for $^{239}\text{Pu}_{\text{th}}$ in kW
- Again Tc 104/5 different feeding for JEFF-3.1.1
- Sr93 jumps by 30% between ENDF and JENDL

Nuclide	ENDF/B-VII.1	Nuclide	JENDL-4.0	Nuclide	JEFF3.2/3.1.1
Tc104	93.8	Tc104	93.8	Tc104	54.9
Tc105	59.5	Tc105	59.6	Sr93	44.6
Mo101	44.5	Mo101	45.9	Mo101	44.5
Sr93	53.6	Sr93	40.6	Y95	29.5
Y95	33.1	Y95	30.0	Xe138	28.7
Xe138	28.8	Xe138	28.8	Cs138	26.9
Cs138	27.0	Cs138	27.0	Ba142	26.7
Ba142	26.7	Ba142	26.5	Tc105	21.8

Different nuclear data # results on dominants ??



Comparison of high resolution (ENSDF) with TAS β -intensity



- In all three cases TAS reveals considerable *Pandemonium* effect

Isotope	$\langle E_\gamma \rangle$ ENSDF	$\langle E_\gamma \rangle$ TAS
87Br	3057 keV	3945 keV
88Br	2861 keV	4591 keV
94Rb	1729 keV	4060 keV

- Impact on reactor decay heat and anti-neutrino spectrum summation calculations

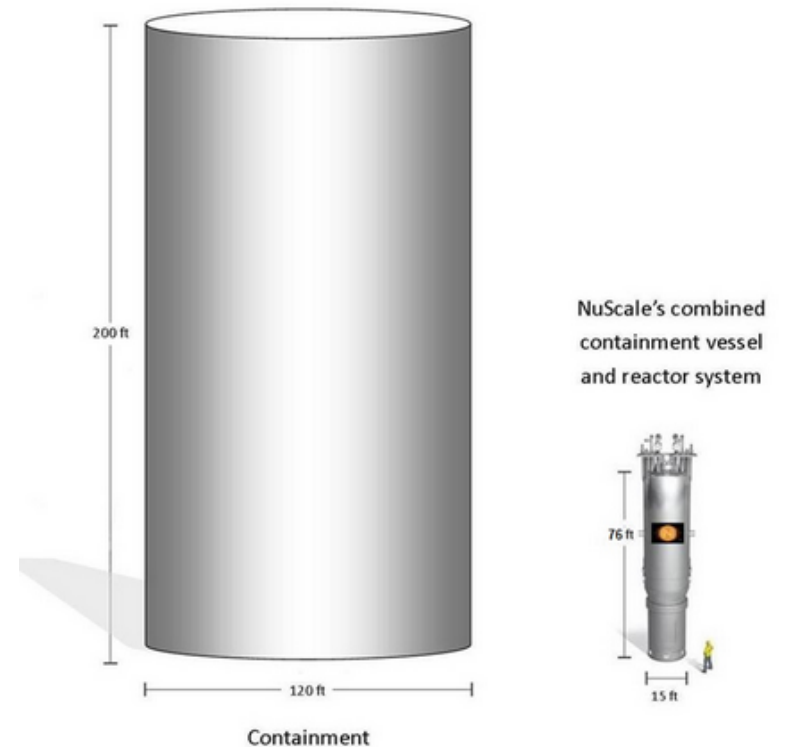
- Certainly not the result of neutrino oscillations but rather a sign that researchers need to know, simulate better the processes that produce antineutrinos:
 - ^{239}Pu versus ^{235}U
 - figure out how the beta decay of each fission product that contributes to the antineutrino spectrum (exchange and screening effects have been demonstrated to have a great influence on the spectrum shape at low energy; better approximation, new measurements, theory for the forbidden non-unique transitions,...)
 - Cumulative FYs and consistent FP decay schemes data
- Why? such predictions could be used in efforts to detect nuclear reactor misuse, as the antineutrino flux and energy depend on the reactor fuel composition

Yesterday and tomorrow trends

- Generation III+ EPR 1,650 Mwe, build on site



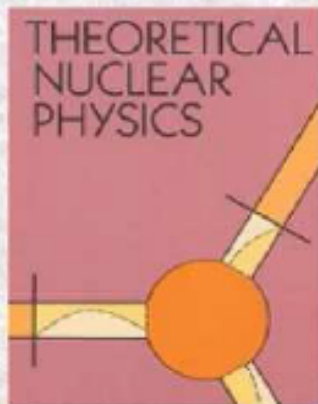
Comparison size envelope of new nuclear plants currently under construction in the United States



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- Small modular reactor, SMR < 300 Mwe, factory build

Today – Tomorrow reactor physics ??



$$(1) \begin{pmatrix} a \\ r_1 \\ r_2 \\ \vdots \\ r_n \end{pmatrix}$$

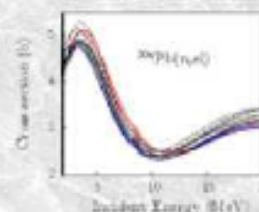
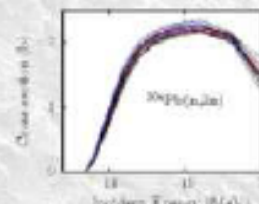
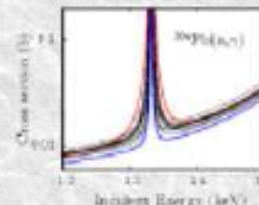
Nuclear Model

Codes

(e.g. TALYS)

$$(2) \begin{pmatrix} a \\ r_1 \\ r_2 \\ \vdots \\ r_n \end{pmatrix}$$

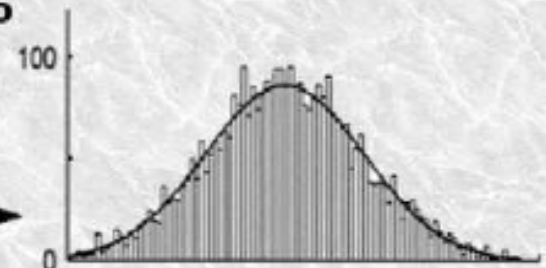
$$(i) \begin{pmatrix} a \\ r_1 \\ r_2 \\ \vdots \\ r_n \end{pmatrix}$$



Monte Carlo

Transport Codes

(e.g. MCNP)



Sensitivity Feedback

(1)

(2)

(3)

Engineers value short turnaround times



Waiting.....

Waiting.....

Waiting.....

Waiting.....

Waiting.....

Waiting.....

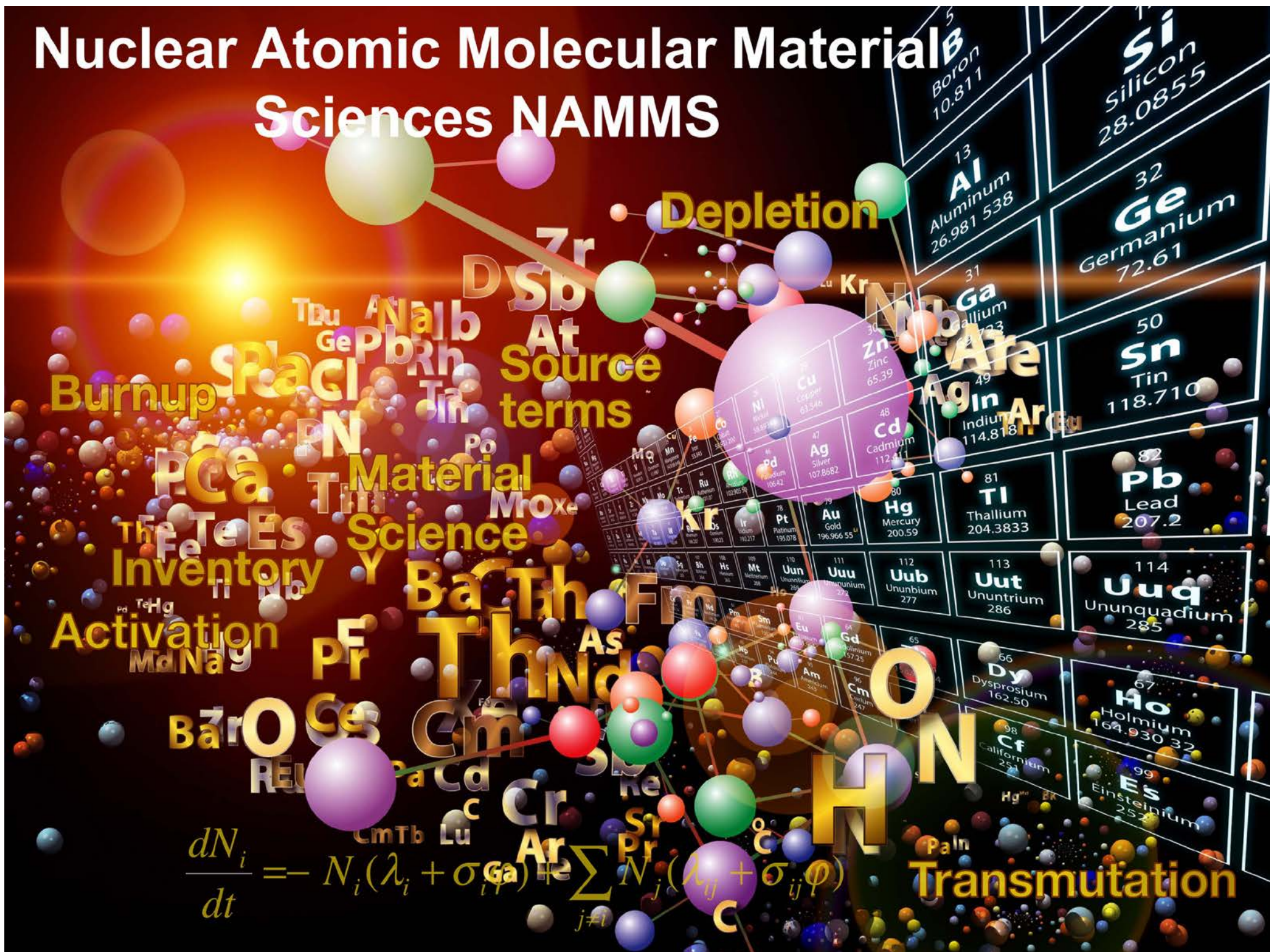
- “Hero runs” are rare: design, analysis, and testing require fast turnaround times
- Real engineering projects require simultaneous execution of many jobs
- Mid-range HPC machines often provide “best” turnaround today
- Most HPC machine queues need to dramatically improve many-user performance

The author would like to acknowledge the influence of the following colleagues in the making of this talk.

Kord Smith (MIT), Muriel Fallot (Mines Nantes), David Lhuillier, Xavier Mougeot, Benjamin Morillon, Pascal Romain, Helder Duarte (CEA), Mark Gilbert, Michael Fleming (UKAEA), Dimitri Rochman (PSI), Arjan Koning (IAEA), Alejandro Sonzogni (BNL), Jose Luis Tain, Alejandro Algora (IFIC), Cyriel Wagemans (JRC), Vladimir Maslov (JINER), Dermott Cullen (LLNL),...

In no particular order

Nuclear Atomic Molecular Material Sciences NAMMS



$$\frac{dN_i}{dt} = -N_i(\lambda_i + \sigma_{i\ell}\phi) + \sum_{j \neq i} N_j(\lambda_{ij} + \sigma_{ij}\phi)$$